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STUDY OF APOLLO WATER IMPACT

FINAL REPORT

VOLUME 5

USER'S MANUAL - NO INTERACTION

(Contract NAS9-4552, G.O. 5264)

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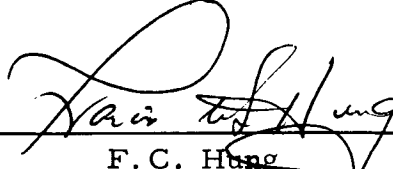
J. P. D. Wilkinson
(Author)

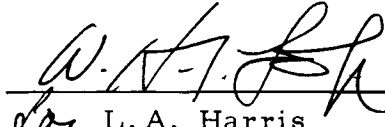
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Approved by


F. C. Hung
Program Manager
Structures and Materials


L. A. Harris
Assistant Manager
Science and Technology

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FOREWORD

This report was prepared by North American Aviation, Inc., Space Division, under NASA Contract NAS9-4552, for the National Aeronautics and Space Administration, Manned Space Flight Center, Houston, Texas, with Dr. F.C. Hung, Program Manager and Mr. P.P. Radkowski, Assistant Program Manager. This work was administered under the direction of Structural Mechanics Division, MSC, Houston, Texas with Dr. F. Stebbins as the technical monitor.

This report is presented in eleven volumes for convenience in handling and distribution. All volumes are unclassified.

The objective of the study was to develop methods and Fortran IV computer programs to determine by the techniques described below, the hydro-elastic response of representation of the structure of the Apollo Command Module immediately following impact on the water. The development of theory, methods and computer programs is presented as Task I Hydrodynamic Pressures, Task II Structural Response and Task III Hydroelastic Response Analysis.

Under Task I - Computing program to extend flexible sphere using the Spencer and Shiffman approach has been developed. Analytical formulation by Dr. Li using nonlinear hydrodynamic theory on structural portion is formulated. In order to cover a wide range of impact conditions, future extensions are necessary in the following items:

- a. Using linear hydrodynamic theory to include horizontal velocity and rotation.
- b. Nonlinear hydrodynamic theory to develop computing program on spherical portion and to develop nonlinear theory on toroidal and conic sections.

Under Task II - Computing program and User's Manual were developed for nonsymmetrical loading on unsymmetrical elastic shells. To fully develop the theory and methods to cover realistic Apollo configuration the following extensions are recommended:

- a. Modes of vibration and modal analysis.
- b. Extension to nonsymmetric short time impulses.

c. Linear buckling and elasto-plastic analysis

These technical extensions will not only be useful for Apollo and future Apollo growth configurations, but they will also be of value to other aeronautical and spacecraft programs.

The hydroelastic response of the flexible shell is obtained by the numerical solution of the combined hydrodynamic and shell equations. The results obtained herein are compared numerically with those derived by neglecting the interaction and applying rigid body pressures to the same elastic shell. The numerical results show that for an axially symmetric impact of the particular shell studied, the interaction between the shell and the fluid produces appreciable differences in the overall acceleration of the center of gravity of the shell, and in the distribution of the pressures and responses. However the maximum responses are within 15% of those produced when the interaction between the fluid and the shell is neglected. A brief summary of results is shown in the abstracts of individual volumes.

The volume number and authors are listed on the following page.

The contractor's designation for this report is SID 67-498.

INDEX FOR FINAL REPORT

"Apollo Water Impact"

<u>Volume No.</u>	<u>Volume Title</u>	<u>Authors</u>
1	Hydrodynamic Analysis of Apollo Water Impact	T. Li and T. Sugimura
2	Dynamic Response of Shells of Revolution During Vertical Impact Into Water - No Interaction	A. P. Cappelli, and J. P. D. Wilkinson
3	Dynamic Response of Shells of Revolution During Vertical Impact Into Water - Hydroelastic Interaction	J. P. D. Wilkinson, A. P. Cappelli, and R. N. Salzman
4	Comparison With Experiments	J. P. D. Wilkinson
5	User's Manual - No Interaction	J. P. D. Wilkinson
6	User's Manual - Interaction	J. P. D. Wilkinson and R. N. Salzman
7	Modification of Shell of Revolution Analysis	A. P. Cappelli and S. C. Furuie
8	Unsymmetric Shell of Revolution Analysis	A. P. Cappelli, T. Nishimoto, P. P. Radkowski and K. E. Pauley
9	Mode Shapes and Natural Frequencies Analysis	A. P. Cappelli
10	User's Manual for Modification of Shell of Revolution Analysis	A. P. Cappelli and S. C. Furuie
11	User's Manual for Unsymmetric Shell of Revolution Analysis	E. Carrion, S. C. Furuie and T. Nishimoto

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ABSTRACT

This volume is a user's manual for a computer program which determines the dynamic response of a shell of revolution during a vertical axially symmetric impact into an incompressible fluid. The program uses the theory developed in Volume 2 of this report where no interaction between the fluid and the flexible shell is accounted for. The hydrodynamic pressures are determined on the basis of a rigid-body theory, and are applied to the shell as a forcing function. The results are intended for comparison with similar calculations derived from Volume 3 and the User's Manual of Volume 6 where the hydroelastic interaction is accounted for.

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CONTENTS

	Page
LIST OF ILLUSTRATIONS	xi
LIST OF TABLES	xi
1.1 INTRODUCTION	1
1.2 Load Map	3
2.1 PROGRAM FLOW DESCRIPTION	9
2.2 Program Deck Setup	13
3.1 RESTART	15
4.1 INPUT DATA FORMAT	17
4.2 DECRD Subroutine	18
4.3 Data Deck Setup	20
4.4 Call DECRD (DA)	21
4.5 Boundary Conditions	22
4.5.1 Top Boundary	22
4.5.2 Bottom Boundary	25
4.6 Call DECRD (GDA).	28
4.7 Call DECRD (CDA).	29
5.1 SAMPLE PROBLEM	33
5.2 Sample Input Data for the Start from Zero	35
5.3 Sample Input Data for the Restart	42
5.4 Sample Output	49
6.1 WARNINGS AND RECOMMENDATIONS	81
6.1.1 Choice of Time Interval	81
6.1.2 Number of Iterations	81
6.1.3 DECRD	81
7.1 PROGRAM LISTINGS	82

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LIST OF ILLUSTRATIONS

Figure		Page
1	Flow of Executive Program 157 DR	10
2	Model of Sample Problem	34

LIST OF TABLES

Table		Page
1	Description of Links	1

1.1 INTRODUCTION

The computer program for the calculation of the dynamic response of shells of revolution during vertical impact into water when no interaction is present is written entirely in FORTRAN IV and makes use of the overlay feature of that language. The program has been checked out in NAASYS, the NAA adaptation of the IBM 7090/7094 IBSYS/IBJOB system; and uses the NAASYS library routines shown in the load map, pages 4 to 8, inclusive, of Section 1.2.

The NAASYS input tape is Unit 5, the output tape is Unit 6. In addition to these files, the program uses Units 8, 9, 10, and 11 as scratch tapes, and Unit 7 as the overlay tape. NAASYS itself is stored on Unit 1.

The program is made up of an executive program and eight links, all of which are called by the executive program. A brief description of each link is shown in Table I below.

Table 1. Description of Links

Link No.	Name	Purpose
0	Executive	Reads general data, DA, and controls flow of execution of other links
1	GEOM	Reads geometric parameters. Prints all geometric input and calculated values
2	CDAFIT	Sets up stiffness parameters
3	ACCN	Computes hydrodynamic pressures on the shell
4	DEFLT	Calculates the deflections due to the pressures
5	PATH	Controls flow after computation of deflections. Computes velocities and accelerations
6	INTLDS	Computes internal loads
7	PSUMS	Outputs all computed quantities
8	PIX	A dummy subroutine for a CRT Plotter

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1.2 Load Map

OVERLAY ORIGIN CARDS AND ASSIGNED LINK NUMBERS

\$ORIGIN	CHAIN	IS LINK	1, PARENT LINK IS	0
\$ORIGIN	CHAIN	IS LINK	2, PARENT LINK IS	0
\$ORIGIN	CHAIN	IS LINK	3, PARENT LINK IS	0
\$ORIGIN	CHAIN	IS LINK	4, PARENT LINK IS	0
\$ORIGIN	CHAIN	IS LINK	5, PARENT LINK IS	0
\$ORIGIN	CHAIN	IS LINK	6, PARENT LINK IS	0
\$ORIGIN	CHAIN	IS LINK	7, PARENT LINK IS	0
\$ORIGIN	CHAIN, SYSUT2, REW	IS LINK	8, PARENT LINK IS	0

* MEMORY MAP *

00000 THRU 03765
03766

SYSTEM
FILE BLOCK ORIGIN

FILES
1. UNIT01
2. UNIT02
3. UNIT03
4. UNIT04
5. UNIT05
6. UNIT06
7. UNIT07
8. UNIT08
9. UNIT09
10. UNIT10
11. UNIT11
12. UNIT12
13. UNIT13
14. UNIT14
15. UNIT15
16. UNIT16

FILE LIST ORIGIN 04266

PRE-EXECUTION INITIALIZATION 04326

CALL CN OBJECT PROGRAM 04373

04400 THRU 37107

LINK DECK ORIGIN CONTROL SECTIONS (/NAME/=NON 0 LENGTH, (LOC)=DELETED, *=NOT REFERENCED)

0	157DR	04400	///	/(51110)	EVEN	04401	*****	05221 *
	MADD	05242	EVEN	05243	MAD	05310		
	MMPY	05351	MMY	05445				
	.LINK	05515	/.LDT /	05515	/.LRECT/	05526	/.LVEC /	05546
	.LXCON	05566	.LXSTR	05566	.LXSTP	05573	.LXOUT	05670
			IBEXIT	05706 *	.LXRTN	05706	.LXCAL	05712 *
			.LXARG	06221	.LO	06240	/TDUMPQ/	06242 *
			.LFBL	06247 *	.LUNB	06250	.DFOUT	06251
			SC.SMT	06254	/SMRI.V/	06255	.OPNFQ	06274
			.WRTFQ	06276	.REDFQ	06277	CNTL..	06300
							.LXERR	05702
							.DBCLS	06100 *
							.CLSE	06246
							CTES..	06253 *
							.CLSFQ	06275

.IODEF	06303	.DEFIN 06303 .READ 06315 .RELES 06341 * .AREAL 06405 .GO 06456 .EX34 06522	.ATTAC 06307 * .WRITE 06317 .LAREA 06352 * .LUNBL 06413 * .DERR 06472 .FPUN 06527	.CLOSE 06311 .BSR 06327 * .LFLBK 06370 .ENTRY 06417 .MOPXI 06476 .PLOT 06527	.OPEN 06313 .READR 06337 * .LTSX 06373 * .GOA 06452 .CUMXI 06500
.IOCSF	06530	.LOVRY (12052) .LXSEL 12624 .LXRCT 12707 * .LYCH 13062 .FFPT. 13102 * OVFLOW 13321 * E.1 13326 CC.1 13332 XIT 13336 FXEM. 13337 RDOPXQ 13766 * FOUT. 14034 FOON. 14375 ENDFS 14450 DBC 14461 DDFIX 14664 DDRS2 15214 * ANPT 15342 DFLT 15530 HOUT 16110 XCF 16354 DONE 17101 QSTO 17177 F808F 17212 MQD 17241 F108. 17262 FRLR. 17527 FBI8F 17633 F10S. 17733 FRTO. 20142	.LDT (05515) .LXSEL 12625 .LXIND 13046 .FPOUT 13236 E.2 13327 CC.2 13333 .EXIT. 13336 .FXOUT 13672 OPEXQ 13770 /HWD SQ / 14425 * .CNVSW 14452 .DBC10 14617 .FIXSW 14672 .D1 15217 .ONPT 15357 .FLT 15665 .INTG 16161 .TEST 17062 .OUTBF 17146 .WIDTH 17200 EVEN 17223 .PEX 17242 .FCNT 17365 .FRLR. (17527) .FRITE 17725 .FSEL. 20122 .FILL. 20150	.LRECT (05526) .LXST 12630 * .LXDIS 13054 .FPARG 13246 E.3 13330 CC.3 13334 .FXARG 13700 /COUNT/ 13250 * E.4 13331 CC.4 13335 /OPTW./ 13754 /NOMSHQ/ 14427 * .FOX1 14456 .DBC20 14645 .DDBC 14747 .D2 15221 .LNT 15442 .DEXPN 15756 .LOUT 16301 .KOUNT 17065 EVEN 17145 .GAIN 17201 .DDDFL 17237 .FEXP 17243 .FBLT. 17463 .FMLR. 17573 .FILR. 20126 * .FCLS 20175 * .FRIB. 20135 .FOPN 20201 *	
.IODEF	12624	.LOVRY 12052 .LXSEL 12624 .LXRCT 12707 * .LYCH 13062 .FFPT. 13102 * OVFLOW 13321 * E.1 13326 CC.1 13332 XIT 13336 FXEM. 13337 RDOPXQ 13766 * FOUT. 14034 FOON. 14375 ENDFS 14450 DBC 14461 DDFIX 14664 DDRS2 15214 * ANPT 15342 DFLT 15530 HOUT 16110 XCF 16354 DONE 17101 QSTO 17177 F808F 17212 MQD 17241 F108. 17262 FRLR. 17527 FBI8F 17633 F10S. 17733 FRTO. 20142	.LDT (05515) .LXSEL 12625 .LXIND 13046 .FPOUT 13236 E.2 13327 CC.2 13333 .EXIT. 13336 .FXOUT 13672 OPEXQ 13770 /HWD SQ / 14425 * .CNVSW 14452 .DBC10 14617 .FIXSW 14672 .D1 15217 .ONPT 15357 .FLT 15665 .INTG 16161 .TEST 17062 .OUTBF 17146 .WIDTH 17200 EVEN 17223 .PEX 17242 .FCNT 17365 .FRLR. (17527) .FRITE 17725 .FSEL. 20122 .FILL. 20150	.LRECT (05526) .LXST 12630 * .LXDIS 13054 .FPARG 13246 E.3 13330 CC.3 13334 .FXARG 13700 /COUNT/ 13250 * E.4 13331 CC.4 13335 /OPTW./ 13754 /NOMSHQ/ 14427 * .FOX1 14456 .DBC20 14645 .DDBC 14747 .D2 15221 .LNT 15442 .DEXPN 15756 .LOUT 16301 .KOUNT 17065 EVEN 17145 .GAIN 17201 .DDDFL 17237 .FEXP 17243 .FBLT. 17463 .FMLR. 17573 .FILR. 20126 * .FCLS 20175 * .FRIB. 20135 .FOPN 20201 *	
.IODEF	17733	.LOVRY 12052 .LXSEL 12624 .LXRCT 12707 * .LYCH 13062 .FFPT. 13102 * OVFLOW 13321 * E.1 13326 CC.1 13332 XIT 13336 FXEM. 13337 RDOPXQ 13766 * FOUT. 14034 FOON. 14375 ENDFS 14450 DBC 14461 DDFIX 14664 DDRS2 15214 * ANPT 15342 DFLT 15530 HOUT 16110 XCF 16354 DONE 17101 QSTO 17177 F808F 17212 MQD 17241 F108. 17262 FRLR. 17527 FBI8F 17633 F10S. 17733 FRTO. 20142	.LDT (05515) .LXSEL 12625 .LXIND 13046 .FPOUT 13236 E.2 13327 CC.2 13333 .EXIT. 13336 .FXOUT 13672 OPEXQ 13770 /HWD SQ / 14425 * .CNVSW 14452 .DBC10 14617 .FIXSW 14672 .D1 15217 .ONPT 15357 .FLT 15665 .INTG 16161 .TEST 17062 .OUTBF 17146 .WIDTH 17200 EVEN 17223 .PEX 17242 .FCNT 17365 .FRLR. (17527) .FRITE 17725 .FSEL. 20122 .FILL. 20150	.LRECT (05526) .LXST 12630 * .LXDIS 13054 .FPARG 13246 E.3 13330 CC.3 13334 .FXARG 13700 /COUNT/ 13250 * E.4 13331 CC.4 13335 /OPTW./ 13754 /NOMSHQ/ 14427 * .FOX1 14456 .DBC20 14645 .DDBC 14747 .D2 15221 .LNT 15442 .DEXPN 15756 .LOUT 16301 .KOUNT 17065 EVEN 17145 .GAIN 17201 .DDDFL 17237 .FEXP 17243 .FBLT. 17463 .FMLR. 17573 .FILR. 20126 * .FCLS 20175 * .FRIB. 20135 .FOPN 20201 *	

		REF	20205 *	REF.Q	20214 *	.IOUT.	20350	.REED	20360 *
		.BIN	20361 *	.FCT	20362	.FCKSZ	20364	SEOF.Q	20405 *
FIOH	20463	.FIOH.	20463	.FFIL.	21250	.FRN.	21275		
FWRD	21473	.FWRD.	21473						
FWRB	21517	.FWRB.	21517						
FRDD	21543	.FRDD.	21543						
FRCB	21571	.FRCB.	21571						
FPUN	21615	/.FPUN/(06527)							
UN01	21754	.UN01.	21754						
UN02	21755	.UN02.	21755						
UN03	21756	.UN03.	21756						
UN04	21757	.UN04.	21757						
UN05	21760	.UN05.	21760						
UN06	21761	.UN06.	21761						
UN07	21765	.UN07.	21765						
UN08	21766	.UN08.	21766						
UN09	21767	.UN09.	21767						
UN10	21770	.UN10.	21770						
UN11	21771	.UN11.	21771						
UN12	21772	.UN12.	21772						
UN13	21773	.UN13.	21773						
UN14	21774	.UN14.	21774						
UN15	21775	.UN15.	21775						
UN16	21776	.UN16.	21776						
FSCD	21777	COSD	21777	SIND	22001				
FSCN	22030	COS	22030	SIN	22031				
FSQR	22224	SQRT	22224						
FRWT	22277	.FRWT.	22277						
FSLDI	22416	.FSLI.	22434	.FSDI.	22442 *				
FSLI	22453	.SLI.	22453	.SLI1.	22460	.SDI.	22466	.SDI1.	22474
FSLD0	22507	.FSLO.	22525	.FSD0.	22533 *				
FSLO	22544	.SLO.	22544	.SLO2.	22552	.SD0.	22557	.SD02.	22566
DECRD	22600	DECRD	(22600)						
FASC	22716	ARCOS	22716 *	ARSIN	22717				
FVIO	23047	.FVIO.	23047						
BCDC8I	23163	/BC.CB./							
//	51110	/CDSEQ /			23263				

1	GENTRY CF3P	23264 33400	/// EVEN	/(51110) 33401	EVEN CODIMA	23265 34414	GEOM	33357
2	CDAFIT CODS ENTP	23264 30037 31200	/// CODIM4 EVEN	/(51110) 31052 31201	EVEN ENTERP	23265 31367	CRVFTT	30021
3	ACCN1 PMAXX	23264 23676	/// EVEN	/(51110) 23677	EVEN PMAXL	23265 23755	ACCN	23634
4	157DR1 MSUB INVR5	23264 36232 36341	/// EVEN INV	/(51110) 36233 37033	EVEN MSU	23265 36300	DEFLTN	36203
5	WHERE	23264	///	/(51110)	EVEN	23265	PATH	24164
6	157DR2	23264	///	/(51110)	EVEN	23265	INTLDS	25421
7	FSUMS	23264	///	/(51110)	EVEN	23265	SUMS	32107
8	LNK6	23264	EVEN	23265	PIX	23300		
I/O BUFFERS								
				37110 THRU	51060			
UNUSED CORE				51061 THRU	51107			
BEGIN EXECUTION				32	00-02-29			

2.1 PROGRAM FLOW DESCRIPTION

An overall flow diagram of the executive program 157DR is shown in Figure 1. A listing of the complete program is shown in Section 7.1.

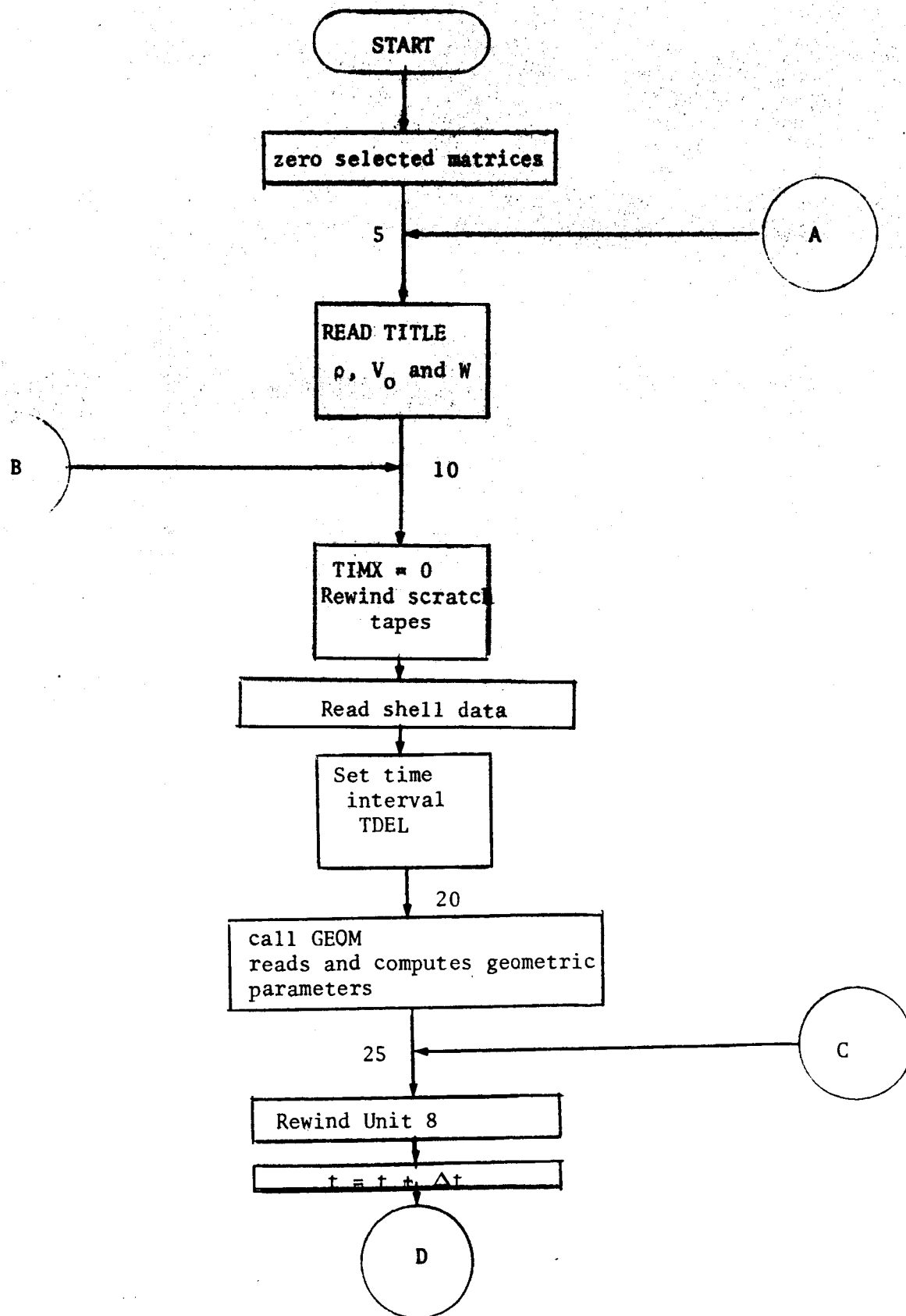


Figure 1. Flow of Executive Program 157 DR (Sheet 1 of 3)

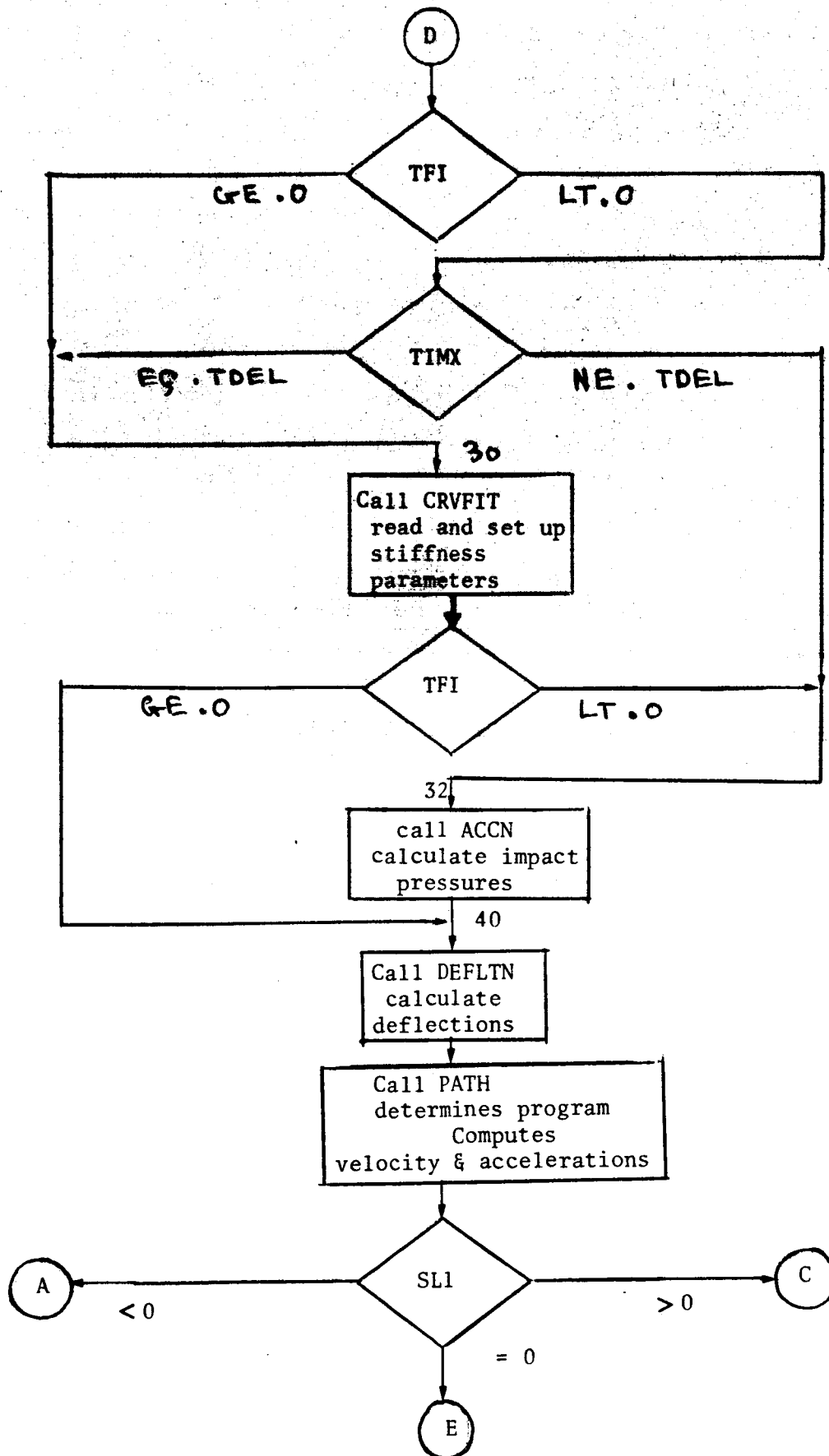


Figure 1. Flow of Executive Program 157 DR (Sheet 2 of 3)

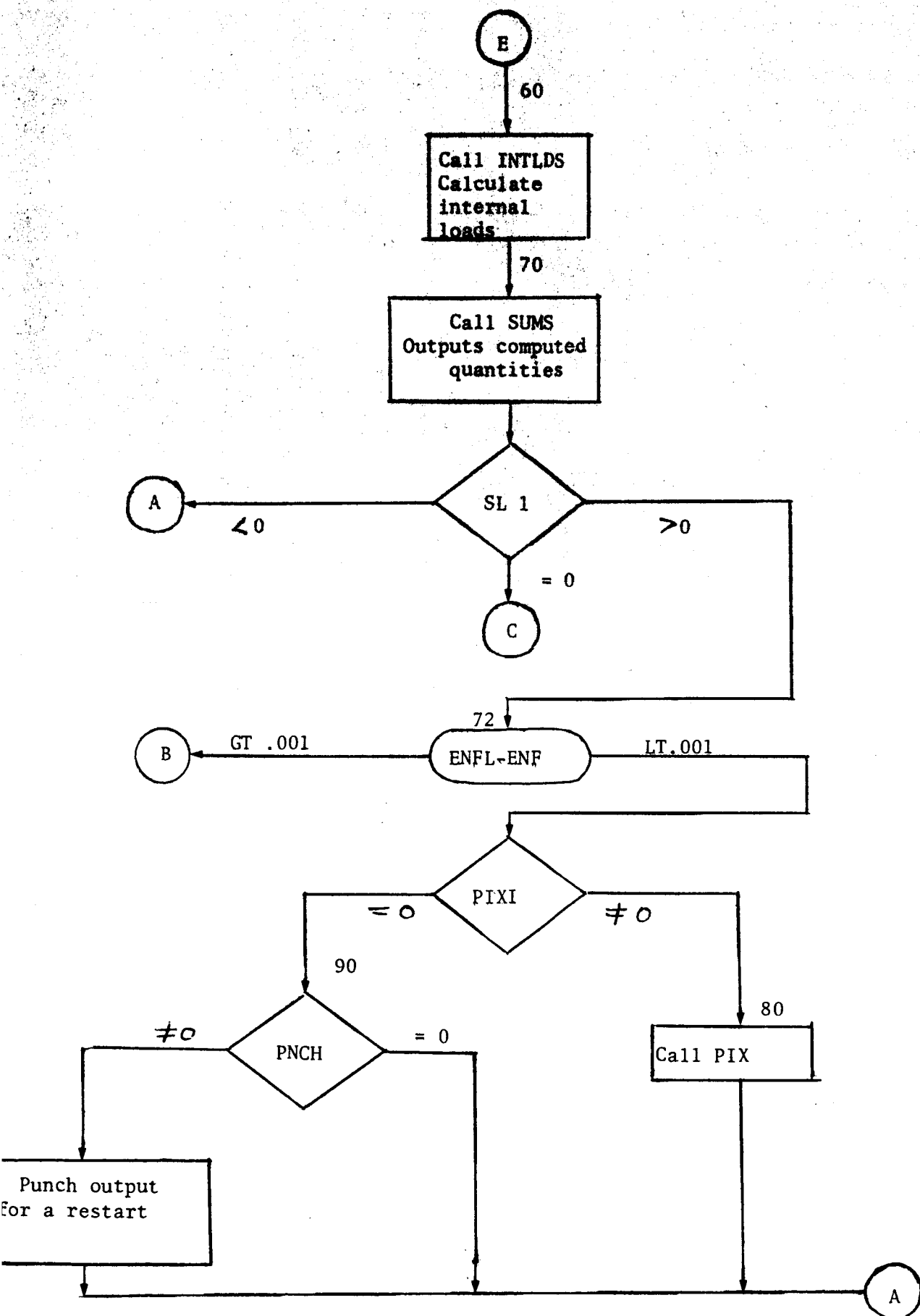


Figure 1. Flow of Executive Program 157 DR (Sheet 3 of 3)

2.2 Program Deck Setup

As explained in Section 1.1, the deck is set up in overlay regions. Each region is denoted by a \$ORIGIN control card. A list of the setup is shown below. It includes the control cards and deck names. The order of these decks must be kept in the given sequence.

Control Cards

Subroutines

\$IBJOB		
\$IBFTC	157 DR	Main program
\$IBFTC	MMPY	MMY
\$IBFTC	MADD	ADD
\$ORIGIN	CHAIN	
\$IBFTC	GMTRY	GEOM
\$IBFTC	CF3P	CODIMA
\$ORIGIN	CHAIN	
\$IBFTC	CDAFIT	CRVFIT
\$IBFTC	CODS	CODIMA
\$IBFTC	ENTP	ENTERP
\$ORIGIN	CHAIN	
\$IBFTC	ACCN2	ACCN
\$IBFTC	PMAXX	PMAXL
\$ORIGIN	CHAIN	
\$IBFTC	157DRI	DEFLT
\$IBFTC	MSUB	MSU
\$IBFTC	INVRS	INV
\$ORIGIN	CHAIN	
\$IBFTC	WHERE	PATH
\$ORIGIN	CHAIN	
\$IBFTC	157DR2	INTLDS
\$ORIGIN	CHAIN	
\$OBFTC	FSUMS	SUMS
\$ORIGIN	CHAIN, SYSUT2, REW	
\$IBFTC	LNK6	PIX
\$DATA		

3.1 RESTART

In many calculations, it may be desired to restart the program at some time t_g without recalculating all the response quantities from zero to t_g . In addition, if it is desired to calculate the response at more than about 120 time intervals, it is necessary to make a restart (see Section 6.1.2).

For a run from zero, the following indicators are set:

RESTRT = 0.0
PNCH = 1.0

Here, the condition RESTRT = 0.0 means that it is a start from zero. The condition PNCH = 1.0 means that at the end of the job certain quantities will be punched on cards to be used as data in a future restart. Thus, part of the output from this job will be some cards containing the arrays

TIMX
ZP(K, L)
Z2P(K, L)
Z3P(K, L)
OMG2(L)

This punching is done by the executive program 157DR.

In order to restart the job, the following indicators are set in the input data:

RESTRT = 1.0
PNCH = 1.0

Here, the condition RESTRT = 1.0 means that the punched output data of the previous job is to be read as input data. The indicator PNCH = 1.0 means that there will also be punched output at the end of this job. If PNCH = 0.0, no data will be punched and no future restart will be possible. The punched cards are put at the end of the data deck. They are read by subroutine CRVFIT.

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4.1 INPUT DATA FORMAT

Data are entered into the program by three subroutines. The executive program 157DR reads the hydrodynamic data, and the DA region of the shell data. Subroutine GEOM reads the GDA region of shell data, and subroutine CDAFIT reads the CDA region of the shell data. The regions DA, GDA, and CDA are read by means of the DECRD subroutine.

The data in regions DA, GDA, and CDA is read by means of the DECRD subroutine. A description of the subroutine follows, together with a listing in FORTRAN IV.

[illegible]

1. **Description.** When a minus sign is encountered in column 1 of a DECRD data card, that card will be read and then reading will be terminated.

The index of a DECRD card must be written to the extreme right of the first 12-column field.

2. Extent: 78 locations.
3. Call Statement:

CALL DECRD (ARRAY)

where ARRAY is the name of the read array to be read. This argument may be subscripted.

4. Error indication: If the index field is zero or blank, the comment "BAD DATA CARD" and the contents of columns 73-80 of the defective card will be printed. The job will be terminated.

5. Example: Assume a CALL DECRD (ARR) statement and the following data cards:

The first card will result in information being stored as follows:

```
ARR(1)  -0.7063E 01
ARR(2)  Unchanged
ARR(3)  0.2435E-00
ARR(4)  0.2065E 04
ARR(5)  0.4649E 04
```

The - sign in column 1 of the second card signals that this is the last card to be read under control of this CALL DECRD statement. This card has been written to illustrate some types of errors (or possible errors) in writing the data. The information will be stored as follows:

ARR(11)	0.7896E 21 (Exponent mislocated or incomplete.)
ARR(12)	Unchanged (Treated as a blank.)
ARR(13)	Unchanged (Treated as a blank.)
ARR(14)	0.2975E 04
ARR(15)	0.1234E 03

When no decimal point is written, as in the last two items, the data is read by the E12,8 format: the number of decimal places is counted from the beginning of the exponent field, if any, or from the extreme right of the field.

\$IBFTC DECRD	DECRD000
SUBROUTINE DECRD(D)	DECRD005
DIMENSION FLT(5), ID(2), D(1)	DECRD010
10 READ (5,100) LOC, FLT, ID	DECRD015
100 FORMAT (I12, 5E12.0, 1A6, 1A2)	DECRD020
IF (LOC.EQ. 0) GO TO 500	DECRD025
15 K = IABS(LOC) - 1	DECRD030
DO 20 I = 1,5	DECRD035
IF (SIGN(1.0,FLT(I)).LT.0.0 .AND. FLT(I) .EQ. 0.0) GO TO 20	DECRD040
J = K + I	DECRD045
D(J) = FLT(I)	DECRD050
20 CONTINUE	DECRD055
IF (LOC.LT. 0) GO TO 1000	DECRD060
GO TO 10	DECRD065
500 WRITE (6,200) ID	DECRD070
200 FORMAT(10H0BAD DATA 1A6,1A2)	DECRD075
CALL EXIT	DECRD080
1000 RETURN	DECRD085
END	DECRD090

4.3 Data Deck Setup

Data decks should be stacked as follows:

1. Three title cards (which may be blank, if necessary).
2. A card with VIN, RHO, WT.
3. DA, general shell data, read by executive program.
4. GDA, geometry data, read by GEOM subroutine.
5. CDA, section properties data, read by CDAFIT subroutine.

The data in groups 3, 4, and 5 should have a minus sign in column 1 of the last card.

The following tables show the nature of the DA, GDA, and CDA decks.

4.4 Call DECRD (DA)

DECRD Index	Name	Description
1	EN	No. of points along shell meridian
2	AO	Reference length (in.)
3	HO	Reference thickness (in.)
4	BO	Reference Young's Modulus (psi)
5	SIGO	Reference stress (psi)
8	POI	Poisson's ratio
11	SPRL	Location of spring along meridian
12	UK	Spring value in ξ direction
14	WK	Spring value in normal direction
16	TAU1	Length of total time interval from zero
17	ENTI	Total no. of time intervals from zero to TAU1
18	PII	Print interval (will always print last interval)
25	MASS	Mass density lbs. sec ² /in ⁴
26	CFE	Coefficient of viscous damping at each station in ξ direction
27	CZ	Coefficient of viscous damping in normal direction.
28	SKFE	Spring constants of shell under elastic restraint in ξ direction
29	SKZ	Spring constant at each station in normal direction
30	SUM	Fourier summing increment (always -1.)
33	TFI	(Always -1)
36	RESTRT	0. for start from zero, 1. for restart
37	PNCH	0. no future restart; 1. restart cards are punched
4440	EMI	See description of top boundary conditions in Section 4.6.
4476	EMIN	See description of bottom boundary conditions in Section 4.6.

For most cases
set to 1.0

Last card must have a - sign in Column 1.

4.5 Boundary Conditions

4.5.1 Top Boundary

When the boundary conditions on the top boundary are of the following kind, a special flag can be used to specify them:

free: $(N_{\xi} = N_{\xi\theta} = \hat{F}_{\xi} = M_{\xi} = 0) = 1.$

roller: $(N_{\xi} = u_{\theta} = W = M_{\xi} = 0) = 2.$

fixed: $(u_{\xi} = u_{\theta} = W = \phi_{\xi} = 0) = 3.$

simply supported: $(u_{\xi} = u_{\theta} = W = M_{\xi} = 0) = 4.$

complete: $(u_{\xi} = u_{\theta} = \hat{F}_{\xi} = \phi_{\xi} = 0) = 5.$

In these cases, DA(4440) = 1. E10, and DA(4441) is given the value 1., 2., 3., 4., or 5. as shown above. Other special boundary conditions may also be specified. As an example, the full boundary (which is also given above) can be specified as shown in the following data sheets.

FORTRAN FIXED IO DIGIT DECIMAL DATA

DECK NO.	PROGRAMMER	DATE	PAGE	of	DESCRIPTION	DO NOT KEY PUNCH
1						
13						
25						
37						
49						
61						
1						
13						
25						
37						
49						
61						
1						
13						
25						
37						
49						
61						

Diagonal Boundary Force Matrix
 EM1(4 X 4), omega at top of shell.

e.g. (free boundary) $\begin{bmatrix} 1 \\ 1 \\ 1 \\ 0 \end{bmatrix}$

EXAMPLE.
 EM1 (contd)

EXAMPLE
 EM1 (contd)

FORTRAN FIXED IO DIGIT DECIMAL DATA

DECK NO.	PROGRAMMER	DATE	PAGE	of	DESCRIPTION	DO NOT KEY PUNCH
1					Diagonal Boundary Displacement Matrix EM3 (4 X 4) Lambda at top of shell e.g. (for free boundary) $\begin{bmatrix} 0 & 0 & 0 & 1 \end{bmatrix}$	
13						
25						
37						
49						
61						
1					EXAMPLE EM3 (cont'd)	
13						
25						
37						
49						
61						
1					Column Boundary Matrix EM5 (4 X 1), L, at top of shell. e.g. $L = \begin{Bmatrix} 0 \\ 0 \\ 0 \\ 0 \end{Bmatrix}$	
13						
25						
37						
49						
61						

4.5.2 Bottom Boundary

The same selection of boundary conditions is available here as for the top boundary. This time, the indicator specifying the free, roller, fixed, simply supported, and complete conditions are set as follows:

DA (4476) = 1. E10

DA (4477) = 1., 2., 3., 4., 5.,

according to the boundary condition desired. An example of other possible boundary conditions is given in the data sheets below. The example here is the free boundary (the same as in Section 4.5.1).

FORTRAN FIXED IO DIGIT DECIMAL DATA

DECK NO. _____ PROGRAMMER _____ DATE _____ PAGE _____ of _____

NUMBER	IDENTIFICATION	DESCRIPTION	DO NOT KEY PUNCH
1		Diagonal Boundary Force Matrix	
13		EMIN(4 X 4) OMEGA at Bottom of shell.	
25			
37			
49		e.g. (fixed boundary)	$\begin{bmatrix} 0 & 0 & 4476 \\ 0 & 0 & 15 \\ 1 & 1 & 7491 \end{bmatrix}$
61			
1		EXAMPLE	
13		EMIN (cont'd)	
25			
37			
49			
61			
1		Diagonal Boundary Displacement Matrix	
13		EM3N(4 X 4) LAMBDA at Bottom of shell.	
25			
37		e.g. (for fixed case).	$\begin{bmatrix} 1 & 1 & 0 \\ 1 & 1 & 1 \\ 0 & 0 & 0 \end{bmatrix}$
49			
61			

FORTRAN FIXED 10 DIGIT DECIMAL DATA

DECK NO. _____		PROGRAMMER _____		DATE _____		PAGE _____ of _____	
NUMBER	IDENTIFICATION	DESCRIPTION	DO NOT KEY PUNCH				
1		EXAMPLE					
13		FMIN (cont'd)					
25							
37							
49							
61							
1		FMIN (cont'd)					
13							
25							
37							
49							
61							
1		Column Boundary Matrix					
13		FMIN (4 X 1), I., at Bottom of shell					
25							
37		e.g. L = { 0 }					
49							
61							

4.6 Call DECRD (CDA)

DECRD Index	Name	Description
1	GMI	Geometry indicator: 1. = cone - cylinder 2. = sphere - toroid 3. = general discrete point 4. = arbitrary functions
2	EN	No. of station points
3	PFLAG	Print indicator; $\neq 0.$, prints all data
4	RA1	For GMI = 1.; radius at station 1
	RC	For GMI = 2.; radius of curvature
5	AXL	For GMI = 1.; axial surface length
	ROFF	For GMI = 2.; off-set distance to center of curvature
6	ANX	For GMI = 1.; angle between generator and axis of revolution
	PHIO	For GMI = 2.; initial opening angle from vertical axis, in degrees.
7	PHIN	For GMI = 2.; final opening angle from vertical axis, in degrees.
8	EM	For GMI = 3.; number of RI points given
9-208	RIPT	For GMI = 3.; discrete radii (200 points maximum)
209-409	XIPT	For GMI = 3.; discrete XI - arc length, (200 points maximum)

The last card must have a - in Column 1.

4.7 Call DECRD (CDA)

The various tables are set up in this region as follows:

TAB (1) = No. of stations given along meridian (i. e. , stations
at which values change).

TAB (2) = Station No. 1.

TAB (3) = Parameter value at Station No. 1

TAB (4) = Next station no.

TAB (5) = Next parameter value

Stations and parameter values interlaced.

The last station must be the Nth station parameter value because
CODIMA interpolation routine will not extrapolate.

If $+1.0 \times 10^{10}$ is placed in TAB (1) the following parameter value is
constant (uniform over all stations EN) and its value is placed in TAB (2).

DECRD Index	Name	Description
		<u>Extensional Rigidity</u>
1	DTB	No. of stations given, if = 1. E10, then a constant extensional rigidity is given in 2
2		Station No. 1. if CDA (1) = 1. E10, then this is a constant value of extensional rigidity.
3		Value of extensional rigidity between Station 1 and next station
4		Station No. 2.
5		Value of extensional rigidity
6-41		Follows same pattern to DTB (20), value of last rigidity.

DECRD Index	Name	Description
		<u>Flexural Rigidity</u>
42	EKTB	No. of stations given, if = 1. E10, then a constant flexural rigidity is given in 43
43		Station No. 1 if CDA (42) = 1. E10, then this is the constant value of flexural rigidity
44		Value of flexural rigidity between station 1 and next station
45		Station No. 2
46		Value of flexural rigidity
47-81		Follows same pattern to EKTB (20), value of last rigidity.
		<u>Continue as above for the following quantities:</u>
83-125	EITB	Young's modulus (E)
124-164	ALFTB	Coefft of thermal expansion (α)
165-205	DNATB	1/2 shell thickness (h/2)
206-246	TTB	Temperature gradient through shell (T)
247-287	ENTB	Membrane thermal load
288-328	EMTB	Bending thermal load
329-369	PNTB	Normal pressure on shell (at reference surface)
370-410	PFBTB	Meridional surface pressure (at reference surface)
452-492	DZOTB	Initial displacement in normal direction.
493-533	VZOTB	Initial velocity in normal direction
534-574	QZOTB	Initial acceleration in normal direction
575-615	DFOTB	Initial displacement in ξ direction
616-655	VFOTB	Initial velocity in ξ direction.
657-691	QFOTB	Initial acceleration in ξ direction.

The last card must have a - sign in Column 1.

5.1 SAMPLE PROBLEM

To demonstrate the use of the computer program, and to illustrate the format of the input and output data, the sample problem shown in Figure 2 has been calculated.

The problem concerns the vertical impact of a flexible body of revolution consisting of a shallow spherical shell to which is rigidly attached a heavier mass so that their combined weight is 10,000 lbs. The radius of curvature of the shell middle surface is 175.6 ins., and the opening angle is 19.53°. The shell extensional and flexural stiffnesses are both set equal to 3.33×10^6 lbs/in., which corresponds to a sandwich shell having 0.05 in. steel facings and 1.95 in. honeycomb core. Other shell properties are as follows: Mass per unit surface area = 9.7×10^{-4} lbs. sec.²/in.³; Poisson's ratio = 0.33, and modulus of elasticity $E = 29.7 \times 10^6$ psi. The initial impact velocity is 30 fps. The hydrodynamic loads are computed on the basis of the rigid-body theory of Volume 2 of this report, and are then applied as a forcing function to the shell of revolution. A full discussion of the numerical results obtained is given in Volume 2. Sample data sheets follow.

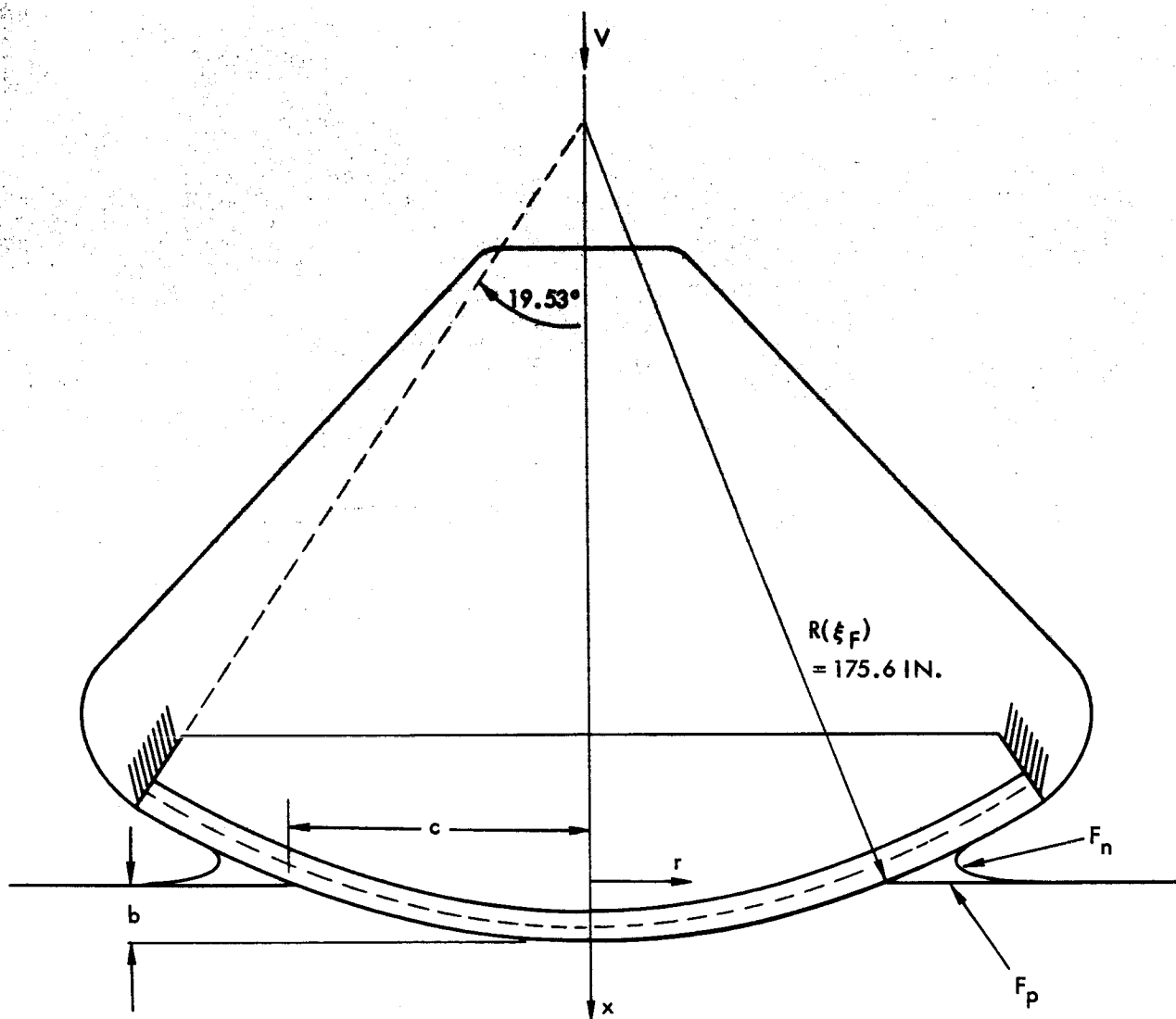


Figure 2. Model of Sample Problem.

5.2 Sample Input Data for a start from zero

In the present problem, we shall use a time interval of .0001 seconds and make a run to 1.0 milliseconds. Because it may, at some future date, be desirable to make a restart at 1.0 ms. (to avoid recalculating the response from zero), we shall punch some quantities on cards to make this restart possible. They will be part of the input in the future restart. Thus we set `RESTR` = 0.0, and `PUNCH` = 1.0.

Sample input sheets are shown below for the start from zero.

FORTRAN FIXED IO DIGIT DECIMAL DATA

DECK NO. _____ PROGRAMMER _____ DATE _____ PAGE _____ of _____ JOB NO. _____

NUMBER	IDENTIFICATION	DESCRIPTION DO NOT KEY PUNCH
1	73 80	T I T L E
13		
25		
37		
49		
61		
1	73 80	T I T L E
13		
25		
37		
49		
61		
1	73 80	T I T L E
13		
25		
37		
49		
61		
1	73 80	Initial Velocity, fps VIN
13		Mass density of fluid, lbs/cu ft RHO
25		Weight of capsule, lbs. WT
37		
49		
61		

FORTRAN FIXED IO DIGIT DECIMAL DATA

DECK NO. _____ PROGRAMMER _____ DATE _____ PAGE _____ of _____

NUMBER	IDENTIFICATION	DESCRIPTION	DO NOT KEY PUNCH
1			
2			
13		AO	
25		HO	
37		EO	
49		SIGQ	
61			
1			
13			
25		POI	
37			
49			
61			
1			
13		TAUL	
25		ENTL	
37		PIU	
49			
61			

FORTRAN	FIXED	IO	DIGIT	DECIMAL	DATA
---------	-------	----	-------	---------	------

DECK NO. _____ PROGRAMMER _____ DATE _____ PAGE _____ of _____

NUMBER		IDENTIFICATION	DESCRIPTION	DO NOT KEY PUNCH
1	2 1			
13				
25				
37				
49				
61	9 7 5 - 3		MASS	
1	3 0			
13	- 1		SUM	
25				
37				
49				
61				
1	3 3			
13	- 1		TFI	
25	3 6 0		VIN	
37				
49	0 0 0		RESTR	
61	1 0 0		PNCH	

FORTRAN FIXED 10 DIGIT DECIMAL DATA

DECK NO. _____ PROGRAMMER _____ DATE _____ PAGE _____ of _____

NUMBER	IDENTIFICATION	DESCRIPTION	DO NOT KEY PUNCH
1 -			
13			
25		EMIN	
37		EM3N	
49			
61			
1			
13			
25		GMI	
37		EN	
49		PFLAG	
61		RC	
1		ROFF	
13			
25		PHIO	
37		PHIN	
49			
61			

FORTRAN FIXED IO DIGIT DECIMAL DATA

DECK NO. _____ PROGRAMMER _____ DATE _____ PAGE _____ of _____

NUMBER	IDENTIFICATION	DESCRIPTION	DO NOT KEY PUNCH
1 1			CDA
13 1 . 0 + 1 0		DTB	
25 3 . 3 3 + 6			
37			
49	73 80		
61			
1 4 2			
13 1 . 0 + 1 0		EKTB	
25 3 . 3 3 + 6			
37			
49	73 80		
61			
1 8 3			
13 1 . 0 + 1 0		EITB	
25 2 9 . 7 + 6			
37			
49	73 80		
61			

FORTRAN FIXED IO DIGIT DECIMAL DATA

DECK NO. _____ PROGRAMMER _____ DATE _____ PAGE _____ of _____

NUMBER		IDENTIFICATION	DESCRIPTION	DO NOT KEY PUNCH
1	-			
13	1 6 5			
25	1 • 0 + 1 0		DNATB	
37	1 • 0 2 5			
49		73 80		
61				
1				
13				
25				
37				
49		73 80		
61				
1				
13				
25				
37				
49		73 80		
61				

5.3 Sample Data for the Restart

In order to restart the problem at 1.0 ms., the following input is required. Note that the time interval must be the same in all runs. The changes in data are indicated by the arrows in the data sheets. Note particularly that RESTRT = 1.0 here. The output cards obtained from the previous run are placed at the end of the data deck. They are read in subroutine CDAFIT.

The output quantities will be identical to those from the start from zero.

FORTRAN FIXED 10 DIGIT DECIMAL DATA

DECK NO.	PROGRAMMER	DATE	PAGE	of	JOB NO.	DESCRIPTION	DO NOT KEY PUNCH
1	T I T L E						
13							
25							
37							
49							
61							
1	T I T L E						
13							
25							
37							
49							
61							
1	T I T L E						
13							
25							
37							
49							
61							
1	3 0 0 0					Initial Velocity, fps	
13	6 2 5					Mass density of fluid, lbs./in ft.	
25	1 0 0 0 0 0					Weight of capsule, lbs	
37							
49							
61							

FORTRAN FIXED 10 DIGIT DECIMAL DATA

DECK NO.	PROGRAMMER	DATE	PAGE	of	DESCRIPTION	DO NOT KEY PUNCH
1	2				A0	Same
13						
25	1.				H0	
37	1.				E0	
49	1.				SIG0	
61						
1	0.0				INFO	
13	7					Same
25	0.0				ENEL	
37	0.3.3				POI	
49	0.0				THETA	
61	0.0				PIXI	
1	1.6					
13	2.0				TAU1	←
25	2.0				ENT1	←
37	1.				PI1	
49						
61						

FORTRAN FIXED IO DIGIT DECIMAL DATA

DECK NO. _____		PROGRAMMER _____		DATE _____		PAGE _____ of _____	
NUMBER	IDENTIFICATION	DESCRIPTION	DO NOT KEY PUNCH				
1			Same				
13							
25							
37							
49							
61							
1							
13							
25							
37							
49							
61							
1							
13							
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FORTRAN FIXED 10 DIGIT DECIMAL DATA

DECK NO. _____ PROGRAMMER _____ DATE _____ PAGE _____ of _____

NUMBER	IDENTIFICATION	DESCRIPTION	DO NOT KEY PUNCH
1 -			Same
13 4 4 7 6			
25 1 9 0 + 1 0		EM1N	
37 3 0 0		EM3N	
49			
61			
1 1			Same
13 2 0 0		GMI	
25 1 2 0 0 0		EN	
37 - 1 0 0		PFLAG	
49 1 7 5 6		RA1, RC	
61 0 0 0		AXL, ROFF	
1 6			Same
13 0 0 0		ANX, PHIO	
25 1 9 5 3 0		PHIN	
37			
49			
61			

FORTRAN FIXED 10 DIGIT DECIMAL DATA

DECK NO. _____		PROGRAMMER _____		DATE _____		PAGE _____ of _____	
NUMBER		IDENTIFICATION		DESCRIPTION		DO NOT KEY PUNCH	
1	1	73	80		DTB		Same
13	+ 1 0						
25	+ 6						
37	1 . 0 .						
49	3 . 3 . 3 .						
61							
1	4 2	73	80		EKTB		Same
13	+ 1 0						
25	1 . 0 .						
37	3 . 3 . 3 .						
49							
61							
1	8 3	73	80		EITB		Same
13	+ 1 0						
25	2 9 . 7 .						
37							
49							
61							

FORTRAN FIXED 10 DIGIT DECIMAL DATA

DECK NO. _____ PROGRAMMER _____ DATE _____ PAGE _____ of _____

NUMBER	IDENTIFICATION	DESCRIPTION DO NOT KEY PUNCH
1 -		Same
13 1.6.5 + 1.0		DNATB
25 1.0.0.2.5		
37		
49	73 80	
61		
1		Set the punched restart cards at this
13		point in the input data deck.
25		
37		
49	73 80	
61		
1		
13		
25		
37		
49	73 80	
61		

5.4 Sample Output

The following pages show the output resulting from the start from zero of the sample problem. Letters in circles correspond to descriptions below.

(A)	First Title Card
(B)	Second Title Card
(C)	Third Title Card
(D)	No. of Stations EN
(E)	Radius of curvature, ins.
(F)	Offset distance from center of curvature = 0
(G)	Closed apex, therefore PHIO initial opening angle is zero
(H)	PHIN, final opening angle is 19.53°
(I)	Station number
(J)	R(I), normal distance from shell to axis
(K)	W(THETA) nondimensional curvature in θ direction
(L)	W(XI) nondimensional curvature in ξ direction
(M)	$RHOX(I) \quad R(I)/AO = \rho/AO$
(N)	$GAMMA(I) \quad \rho'/\rho$
(O)	DTB, the extensional rigidity (constant over shell)
(P)	EKTB, the flexural rigidity (constant over shell)
(Q)	EITB, the Young's modulus (constant over shell)
(R)	ALFTB, thermal expansion coefficient (zero)
(S)	DNATB, 1/2 shell thickness (constant over shell)
(T)	TTB, temperature gradient (zero)

U	ENTB, membrane thermal load (zero)
V	EMTB, bending thermal load (zero)
W	All these other quantities, read by CDR, are set to zero.
X	See Sections 4.4 to 4.7 for descriptions
EN	= number of stations
AO	= reference length
HO	= Reference thickness
EO	= Reference Young's modulus
SIGO	= Reference stress level
ENFO	= always zero
ENFL	= always zero
POI	= Poisson's ratio
THETA	= always zero
PIXI	= always zero
SPRL	= location of spring along meridian
UK	= spring value in ξ direction
VK	= always zero
WK	= spring value in normal direction
EMK	= always zero
TAU1	= total length of time from zero
ENT1	= Total no. of time intervals from zero to TAU1
PI1	= point interval. Here PI1 = 1, and output is pointed at end of enc interval

TAU2	= 0	} (always zero)
ENT2	= 0	
PI2	= 0	
TAU3	= 0	
ENT3	= 0	

PI3 = 0

MASS = mass density

CFE = coefficient of viscous damping at each station in direction

CZ = coefficient of viscous damping at each station in normal direction

SKFE = spring constant of shell under elastic restraining in direction

SUM = - 1. always

EN1 = 1., open shell; = 2., closed shell; set in GEOM

DEL = distance between station points

BCITP = boundary condition indicator - top boundary

BCIBM = boundary condition indicator - bottom boundary

Y Full Tables of

D Extensional rigidity

EK Flexural rigidity

E1 Young's modulus

ALF Coefficient of thermal expansion (zero here)

DNA $\frac{1}{2}$ shell thickness

T	temperature gradient through shell (zero here)
ENT	membrane thermal load (zero here)
EMT	bending thermal load (zero here)
(Z)	Full Tables of PN, PFE, DZO, VZO, AZO, DFO, VFO, AFO, all of which were read as zero in CDA. [See Section 4.7 for their descriptions].
(BA)	is self-explanatory. It shows the time (t), maximum radius of the pressure profile (c), and overall vehicle velocity (V). Maximum pressure is given in BC, and depth submerged is not computed here.
(BB)	is a column showing the station number from the apex (1) to the boundary (120).
(BC)	is a column of the total pressure acting at each station point. Because the maximum radius of the wetted surface is 3.56 ins., and the distance between each station point (DEL, see (X)) is .503 ins., the wetted surface only extends to station 8. Beyond this station, no pressure is applied. Note that the maximum pressure always occurs at the edge of the wetted surface, in this case at station 8.
(CA)	This page contains columns of response output. The columns are as follows:
I	Station points along shell meridian
U(I)	Tangential displacement (ins) of middle surface in ξ direction
V(I)	Tangential displacement of middle surface in θ direction. Here zero because problem is axially symmetric.
W(I)	Transverse displacement (ins.) of middle surface (positive outward).
M(PHI)	Meridional bending moment M_{ξ} (in lbs/in.)
M(THETA)	Circumferential bending moment M_{θ} (in lbs./in.)
M(PHI, THETA)	Twisting moment $M_{\xi\theta}$. Zero here because problem is axially symmetric.
Q(PHI)	Shear force Q_{ξ} (lbs/in.)

Q(THETA)	Shear force Q_θ . Zero here because problem is axially symmetric.
ⒹⒶ	Additional columns of response.
I	Station point along meridian
N(PHI)	Meridional membrane force N_ξ (lbs/in.)
N(THETA)	Circumferential membrane force N_θ (lbs/in.)
N(PHI, THETA)	Twisting force $N_{\xi\theta}$. Zero here because problem is axially symmetric.
SIG(PHI)	Stress σ_ξ (psi) on outer fiber of shell.
SIG (THETA)	Stress σ_θ (psi) on outer fiber of shell.
SIG(PHI, THETA)	Stress $\sigma_{\xi\theta}$ on outer fiber of shell. Zero here because problem is axisymmetric.
ⒷⒶ	Additional columns of response.
VEL(U)	Tangential velocity in ξ direction (ins./sec.)
VEL(V)	Tangential velocity in θ direction. Zero here because problem is axially symmetric
VEL(W)	Transverse velocity (ins/sec.), positive in outward direction.
ACC(U)	Tangential acceleration in ξ direction (ins./sec ²)
ACC(V)	Tangential acceleration in θ direction (ins./sec ²)
ACC(W)	Transverse acceleration (ins./sec ²), positive in outward direction.

(A) DYNAMIC RESPONSE OF APOLLO C/M - NO INTERACTION

(B) V=30 FPS, WT=10000 LBS,

(C) SAME SHELL AS THE HYDROELASTIC CASE

GEOMETRY DATA FOR REGION... (SPHERE - TOROID)

NUMBER OF STATIONS - 120

RC = 1.7560E 02 (E) ROFF = 0.0000E-39 (F) PHIO = 0.0000E-39 (G) PHIN = 1.9530E 01 (H)

(I)	(J)	R(I)	(K)	W(THETA)	(L)	W(XI)	(M)	RHO(XI)	(N)	GAMMA(I)
1		0.0000000E-39		5.6947608E-03		5.6947608E-03		0.0000000E-39		1.0000000E 10
2		5.0298677E-01		5.6947608E-03		5.6947608E-03		5.0298677E-01		1.9881132E 00
3		1.0059694E 00		5.6947608E-03		5.6947608E-03		1.0059694E 00		9.9404982E-01
4		1.5089438E 00		5.6947608E-03		5.6947608E-03		1.5089438E 00		6.6269082E-01
5		2.0119058E 00		5.6947608E-03		5.6947608E-03		2.0119058E 00		4.9700860E-01
6		2.5148512E 00		5.6947608E-03		5.6947608E-03		2.5148512E 00		3.9759707E-01
7		3.0177760E 00		5.6947608E-03		5.6947608E-03		3.0177760E 00		3.3132092E-01
8		3.5206761E 00		5.6947608E-03		5.6947608E-03		3.5206761E 00		2.8397928E-01
9		4.0235473E 00		5.6947608E-03		5.6947608E-03		4.0235473E 00		2.4847166E-01
10		4.5263854E 00		5.6947608E-03		5.6947608E-03		4.5263854E 00		2.2085342E-01
11		5.0291864E 00		5.6947608E-03		5.6947608E-03		5.0291864E 00		1.9875776E-01
12		5.5319462E 00		5.6947608E-03		5.6947608E-03		5.5319462E 00		1.8067849E-01
13		6.0346605E 00		5.6947608E-03		5.6947608E-03		6.0346605E 00		1.6561151E-01
14		6.5373253E 00		5.6947608E-03		5.6947608E-03		6.5373253E 00		1.5286171E-01
15		7.0399365E 00		5.6947608E-03		5.6947608E-03		7.0399365E 00		1.4193255E-01
16		7.5424901E 00		5.6947608E-03		5.6947608E-03		7.5424901E 00		1.3245986E-01
17		8.0449816E 00		5.6947608E-03		5.6947608E-03		8.0449816E 00		1.2417057E-01
18		8.5474072E 00		5.6947608E-03		5.6947608E-03		8.5474072E 00		1.1685585E-01
19		9.0497625E 00		5.6947608E-03		5.6947608E-03		9.0497625E 00		1.1035329E-01
20		9.5520437E 00		5.6947608E-03		5.6947608E-03		9.5520437E 00		1.0453462E-01
21		1.0054246E 01		5.6947608E-03		5.6947608E-03		1.0054246E 01		9.9297290E-02
22		1.0556367E 01		5.6947608E-03		5.6947608E-03		1.0556367E 01		9.4558232E-02
23		1.1058400E 01		5.6947608E-03		5.6947608E-03		1.1058400E 01		9.0249507E-02
24		1.1560343E 01		5.6947608E-03		5.6947608E-03		1.1560343E 01		8.6314971E-02
25		1.2062191E 01		5.6947608E-03		5.6947608E-03		1.2062191E 01		8.2707830E-02
26		1.2563940E 01		5.6947608E-03		5.6947608E-03		1.2563940E 01		7.938867E-02
27		1.3065586E 01		5.6947608E-03		5.6947608E-03		1.3065586E 01		7.6324775E-02
28		1.3567125E 01		5.6947608E-03		5.6947608E-03		1.3567125E 01		7.3487252E-02
29		1.4068553E 01		5.6947608E-03		5.6947608E-03		1.4068553E 01		7.0852008E-02
30		1.4569865E 01		5.6947608E-03		5.6947608E-03		1.4569865E 01		6.8398137E-02
31		1.5071057E 01		5.6947608E-03		5.6947608E-03		1.5071057E 01		6.6107531E-02
32		1.5572126E 01		5.6947608E-03		5.6947608E-03		1.5572126E 01		6.3964297E-02
33		1.6073067E 01		5.6947608E-03		5.6947608E-03		1.6073067E 01		6.1954680E-02
34		1.6573876E 01		5.6947608E-03		5.6947608E-03		1.6573876E 01		6.0066543E-02
35		1.7074549E 01		5.6947608E-03		5.6947608E-03		1.7074549E 01		5.8289171E-02

36	1.7575083E 01	5.6947608E-03	5.6947608E-03	1.7575083E 01	5.6613040E-02
37	1.8075472E 01	5.6947608E-03	5.6947608E-03	1.8075472E 01	5.5029696E-02
38	1.8575712E 01	5.6947608E-03	5.6947608E-03	1.8575712E 01	5.3531669E-02
39	1.9075800E 01	5.6947608E-03	5.6947608E-03	1.9075800E 01	5.2112206E-02
40	1.9575732E 01	5.6947608E-03	5.6947608E-03	1.9575732E 01	5.076527E-02
41	2.0C75503E 01	5.6947608E-03	5.6947608E-03	2.0075503E 01	4.9485347E-02
42	2.0575110E 01	5.6947608E-03	5.6947608E-03	2.0575110E 01	4.8267643E-02
43	2.1074547E 01	5.6947608E-03	5.6947608E-03	2.1074547E 01	4.7107619E-02
44	2.1573812E 01	5.6947608E-03	5.6947608E-03	2.1573812E 01	4.6001336E-02
45	2.2072900E 01	5.6947608E-03	5.6947608E-03	2.2072900E 01	4.4945092E-02
46	2.2571806E 01	5.6947608E-03	5.6947608E-03	2.2571806E 01	4.3935510E-02
47	2.3070527E 01	5.6947608E-03	5.6947608E-03	2.3070527E 01	4.2969620E-02
48	2.3569060E 01	5.6947608E-03	5.6947608E-03	2.3569060E 01	4.2044602E-02
49	2.4067398E 01	5.6947608E-03	5.6947608E-03	2.4067398E 01	4.1157877E-02
50	2.4565540E 01	5.6947608E-03	5.6947608E-03	2.4565540E 01	4.0307115E-02
51	2.5063479E 01	5.6947608E-03	5.6947608E-03	2.5063479E 01	3.9490150E-02
52	2.5561213E 01	5.6947608E-03	5.6947608E-03	2.5561213E 01	3.8705051E-02
53	2.6058737E 01	5.6947608E-03	5.6947608E-03	2.6058737E 01	3.7949939E-02
54	2.6556047E 01	5.6947608E-03	5.6947608E-03	2.6556047E 01	3.7223095E-02
55	2.7053140E 01	5.6947608E-03	5.6947608E-03	2.7053140E 01	3.6522946E-02
56	2.7550010E 01	5.6947608E-03	5.6947608E-03	2.7550010E 01	3.5848083E-02
57	2.8046654E 01	5.6947608E-03	5.6947608E-03	2.8046654E 01	3.5197140E-02
58	2.8543068E 01	5.6947608E-03	5.6947608E-03	2.8543068E 01	3.4568833E-02
59	2.9039249E 01	5.6947608E-03	5.6947608E-03	2.9039249E 01	3.3961993E-02
60	2.9535190E 01	5.6947608E-03	5.6947608E-03	2.9535190E 01	3.3375551E-02
61	3.0030890E 01	5.6947608E-03	5.6947608E-03	3.0030890E 01	3.2808464E-02
62	3.0526343E 01	5.6947608E-03	5.6947608E-03	3.0526343E 01	3.2259780E-02
63	3.1021546E 01	5.6947608E-03	5.6947608E-03	3.1021546E 01	3.1728643E-02
64	3.1516494E 01	5.6947608E-03	5.6947608E-03	3.1516494E 01	3.1214161E-02
65	3.2011183E 01	5.6947608E-03	5.6947608E-03	3.2011183E 01	3.0715596E-02
66	3.2505610E 01	5.6947608E-03	5.6947608E-03	3.2505610E 01	3.0232233E-02
67	3.2999770E 01	5.6947608E-03	5.6947608E-03	3.2999770E 01	2.9763296E-02
68	3.3493659E 01	5.6947608E-03	5.6947608E-03	3.3493659E 01	2.9308242E-02
69	3.3987274E 01	5.6947608E-03	5.6947608E-03	3.3987274E 01	2.886410E-02
70	3.4480610E 01	5.6947608E-03	5.6947608E-03	3.4480610E 01	2.8437188E-02
71	3.4973663E 01	5.6947608E-03	5.6947608E-03	3.4973663E 01	2.8020073E-02
72	3.5466428E 01	5.6947608E-03	5.6947608E-03	3.5466428E 01	2.7614568E-02
73	3.5958903E 01	5.6947608E-03	5.6947608E-03	3.5958903E 01	2.7220190E-02
74	3.6451083E 01	5.6947608E-03	5.6947608E-03	3.6451083E 01	2.6836447E-02
75	3.6942964E 01	5.6947608E-03	5.6947608E-03	3.6942964E 01	2.6462908E-02
76	3.7434541E 01	5.6947608E-03	5.6947608E-03	3.7434541E 01	2.6099197E-02
77	3.7925812E 01	5.6947608E-03	5.6947608E-03	3.7925812E 01	2.5744945E-02
78	3.8416771E 01	5.6947608E-03	5.6947608E-03	3.8416771E 01	2.5399712E-02

79	3.8907415E 01	5.6947608E-03	5.6947608E-03	3.8907415E 01	2.5063192E-02
80	3.9397740E 01	5.6947608E-03	5.6947608E-03	3.9397740E 01	2.4735048E-02
81	3.9887742E 01	5.6947608E-03	5.6947608E-03	3.9887742E 01	2.4414981E-02
82	4.0377416E 01	5.6947608E-03	5.6947608E-03	4.0377416E 01	2.4102696E-02
83	4.0866759E 01	5.6947608E-03	5.6947608E-03	4.0866759E 01	2.3797857E-02
84	4.1355767E 01	5.6947608E-03	5.6947608E-03	4.1355767E 01	2.3500226E-02
85	4.1844435E 01	5.6947608E-03	5.6947608E-03	4.1844435E 01	2.3209592E-02
86	4.2332760E 01	5.6947608E-03	5.6947608E-03	4.2332760E 01	2.2925661E-02
87	4.2820738E 01	5.6947608E-03	5.6947608E-03	4.2820738E 01	2.2648175E-02
88	4.3308365E 01	5.6947608E-03	5.6947608E-03	4.3308365E 01	2.2376920E-02
89	4.3795635E 01	5.6947608E-03	5.6947608E-03	4.3795635E 01	2.2111743E-02
90	4.4282547E 01	5.6947608E-03	5.6947608E-03	4.4282547E 01	2.1852427E-02
91	4.4769096E 01	5.6947608E-03	5.6947608E-03	4.4769096E 01	2.1598686E-02
92	4.5255277E 01	5.6947608E-03	5.6947608E-03	4.5255277E 01	2.1350413E-02
93	4.5741087E 01	5.6947608E-03	5.6947608E-03	4.5741087E 01	2.1107439E-02
94	4.6226521E 01	5.6947608E-03	5.6947608E-03	4.6226521E 01	2.0869563E-02
95	4.6711577E 01	5.6947608E-03	5.6947608E-03	4.6711577E 01	2.0636627E-02
96	4.7196249E 01	5.6947608E-03	5.6947608E-03	4.7196249E 01	2.0408472E-02
97	4.7680534E 01	5.6947608E-03	5.6947608E-03	4.7680534E 01	2.0184968E-02
98	4.8164428E 01	5.6947608E-03	5.6947608E-03	4.8164428E 01	1.9965908E-02
99	4.8647925E 01	5.6947608E-03	5.6947608E-03	4.8647925E 01	1.9751240E-02
100	4.9131024E 01	5.6947608E-03	5.6947608E-03	4.9131024E 01	1.9540828E-02
101	4.9613720E 01	5.6947608E-03	5.6947608E-03	4.9613720E 01	1.9334477E-02
102	5.0096010E 01	5.6947608E-03	5.6947608E-03	5.0096010E 01	1.9132114E-02
103	5.0577888E 01	5.6947608E-03	5.6947608E-03	5.0577888E 01	1.8933587E-02
104	5.1059351E 01	5.6947608E-03	5.6947608E-03	5.1059351E 01	1.8738832E-02
105	5.1540396E 01	5.6947608E-03	5.6947608E-03	5.1540396E 01	1.8547681E-02
106	5.2021016E 01	5.6947608E-03	5.6947608E-03	5.2021016E 01	1.8360069E-02
107	5.2501211E 01	5.6947608E-03	5.6947608E-03	5.2501211E 01	1.8175935E-02
108	5.2980975E 01	5.6947608E-03	5.6947608E-03	5.2980975E 01	1.7995102E-02
109	5.3460304E 01	5.6947608E-03	5.6947608E-03	5.3460304E 01	1.7817525E-02
110	5.3939195E 01	5.6947608E-03	5.6947608E-03	5.3939195E 01	1.7643085E-02
111	5.4417642E 01	5.6947608E-03	5.6947608E-03	5.4417642E 01	1.7471705E-02
112	5.4895643E 01	5.6947608E-03	5.6947608E-03	5.4895643E 01	1.7303353E-02
113	5.5373195E 01	5.6947608E-03	5.6947608E-03	5.5373195E 01	1.7137886E-02
114	5.5850291E 01	5.6947608E-03	5.6947608E-03	5.5850291E 01	1.6975232E-02
115	5.6326930E 01	5.6947608E-03	5.6947608E-03	5.6326930E 01	1.6815336E-02
116	5.6803105E 01	5.6947608E-03	5.6947608E-03	5.6803105E 01	1.6658134E-02
117	5.7278816E 01	5.6947608E-03	5.6947608E-03	5.7278816E 01	1.6503576E-02
118	5.7754057E 01	5.6947608E-03	5.6947608E-03	5.7754057E 01	1.6351507E-02
119	5.8228823E 01	5.6947608E-03	5.6947608E-03	5.8228823E 01	1.6201908E-02
120	5.8703112E 01	5.6947608E-03	5.6947608E-03	5.8703112E 01	1.6054856E-02

CURVE FIT TABLES

[illegible]

37	0.000E-39	0.000E-39	0.000E-39	0.000E-39	0.000E-39	0.000E-39
38	0.000E-39	0.000E-39	0.000E-39	0.000E-39	0.000E-39	0.000E-39
39	0.000E-39	0.000E-39	0.000E-39	0.000E-39	0.000E-39	0.000E-39
40	0.000E-39	0.000E-39	0.000E-39	0.000E-39	0.000E-39	0.000E-39
41	0.000E-39	0.000E-39	0.000E-39	0.000E-39	0.000E-39	0.000E-39

[illegible]

(X)

INITIAL DATA

EN	=	1.200E 02	A0	=	1.000E 00	H0	=	1.000E 00	E0	=	1.000E 00
SIGO	=	1.000E 00	ENFO	=	0.000E-39	ENFL	=	0.000E-39	POI	=	3.300E-01
THETA	=	0.000E-39	PIXI	=	0.000E-39	SPRL	=	0.000E-39	UK	=	0.000E-39
VK	=	0.000E-39	WK	=	0.000E-39	EMK	=	0.000E-39	TAU1	=	1.000E-03
ENT1	=	1.000E 01	PI1	=	1.000E 00	TAU2	=	0.000E-39	ENT2	=	0.000E-39
PI2	=	0.000E-39	TAU3	=	0.000E-39	ENT3	=	0.000E-39	PI3	=	0.000E-39
MASS	=	9.750E-04	CFE	=	0.000E-39	CZ	=	0.000E-39	SKFE	=	0.000E-39
SKZ	=	0.000E-39	SUM	=	-1.000E 00	EN1	=	2.000E 00	DEL	=	5.030E-01

BCITP = 0.000E-39 BCIBM = 3.000E 00

(7)

	D	EK	E1	ALF	DNA	T	ENT	EMT
1	3.330E 06	3.330E 06	2.970E 07	0.000E-39	1.025E 00	0.000E-39	0.000E-39	0.000E-39
2	3.330E 06	3.330E 06	2.970E 07	0.000E-39	1.025E 00	0.000E-39	0.000E-39	0.000E-39
3	3.330E 06	3.330E 06	2.970E 07	0.000E-39	1.025E 00	0.000E-39	0.000E-39	0.000E-39
4	3.330E 06	3.330E 06	2.970E 07	0.000E-39	1.025E 00	0.000E-39	0.000E-39	0.000E-39
5	3.330E 06	3.330E 06	2.970E 07	0.000E-39	1.025E 00	0.000E-39	0.000E-39	0.000E-39
6	3.330E 06	3.330E 06	2.970E 07	0.000E-39	1.025E 00	0.000E-39	0.000E-39	0.000E-39
7	3.330E 06	3.330E 06	2.970E 07	0.000E-39	1.025E 00	0.000E-39	0.000E-39	0.000E-39
8	3.330E 06	3.330E 06	2.970E 07	0.000E-39	1.025E 00	0.000E-39	0.000E-39	0.000E-39
9	3.330E 06	3.330E 06	2.970E 07	0.000E-39	1.025E 00	0.000E-39	0.000E-39	0.000E-39
10	3.330E 06	3.330E 06	2.970E 07	0.000E-39	1.025E 00	0.000E-39	0.000E-39	0.000E-39
11	3.330E 06	3.330E 06	2.970E 07	0.000E-39	1.025E 00	0.000E-39	0.000E-39	0.000E-39
12	3.330E 06	3.330E 06	2.970E 07	0.000E-39	1.025E 00	0.000E-39	0.000E-39	0.000E-39
13	3.330E 06	3.330E 06	2.970E 07	0.000E-39	1.025E 00	0.000E-39	0.000E-39	0.000E-39
14	3.330E 06	3.330E 06	2.970E 07	0.000E-39	1.025E 00	0.000E-39	0.000E-39	0.000E-39
15	3.330E 06	3.330E 06	2.970E 07	0.000E-39	1.025E 00	0.000E-39	0.000E-39	0.000E-39
16	3.330E 06	3.330E 06	2.970E 07	0.000E-39	1.025E 00	0.000E-39	0.000E-39	0.000E-39
17	3.330E 06	3.330E 06	2.970E 07	0.000E-39	1.025E 00	0.000E-39	0.000E-39	0.000E-39
18	3.330E 06	3.330E 06	2.970E 07	0.000E-39	1.025E 00	0.000E-39	0.000E-39	0.000E-39
19	3.330E 06	3.330E 06	2.970E 07	0.000E-39	1.025E 00	0.000E-39	0.000E-39	0.000E-39

LOADS OUTPUT FROM ACCN SUBROUTINE

(13A)

MAX RAD. OF PRESSURE PROFILE = 3.5557E 00

TIME = 1.0000E-04

NORMAL PRESSURES (PN)

(13B)

PN

1	3.8107E 02
2	3.8494E 02
3	3.9732E 02
4	4.2089E 02
5	4.6227E 02
6	5.3923E 02
7	7.2098E 02
8	1.0891E 03
9	0.0000E-39
10	0.0000E-39
11	0.0000E-39
12	0.0000E-39
13	0.0000E-39
14	0.0000E-39
15	0.0000E-39
16	0.0000E-39
17	0.0000E-39
18	0.0000E-39
19	0.0000E-39
20	0.0000E-39
21	0.0000E-39
22	0.0000E-39
23	0.0000E-39
24	0.0000E-39
25	0.0000E-39
26	0.0000E-39
27	0.0000E-39

28	0.0000E-39
29	0.0000E-39
30	0.0000E-39
31	0.0000E-39
32	0.0000E-39
33	0.0000E-39
34	0.0000E-39
35	0.0000E-39
36	0.0000E-39
37	0.0000E-39
38	0.0000E-39
39	0.0000E-39
40	0.0000E-39
41	0.0000E-39
42	0.0000E-39
43	0.0000E-39
44	0.0000E-39
45	0.0000E-39
46	0.0000E-39
47	0.0000E-39
48	0.0000E-39
49	0.0000E-39
50	0.0000E-39
51	0.0000E-39
52	0.0000E-39
53	0.0000E-39
54	0.0000E-39
55	0.0000E-39
56	0.0000E-39
57	0.0000E-39
58	0.0000E-39
59	0.0000E-39
60	0.0000E-39
61	0.0000E-39
62	0.0000E-39
63	0.0000E-39
64	0.0000E-39
65	0.0000E-39
66	0.0000E-39
67	0.0000E-39
68	0.0000E-39
69	0.0000E-39
70	0.0000E-39

71	0.0000E-39
72	0.0000E-39
73	0.0000E-39
74	0.0000E-39
75	0.0000E-39
76	0.0000E-39
77	0.0000E-39
78	0.0000E-39
79	0.0000E-39
80	0.0000E-39
81	0.0000E-39
82	0.0000E-39
83	0.0000E-39
84	0.0000E-39
85	0.0000E-39
86	0.0000E-39
87	0.0000E-39
88	0.0000E-39
89	0.0000E-39
90	0.0000E-39
91	0.0000E-39
92	0.0000E-39
93	0.0000E-39
94	0.0000E-39
95	0.0000E-39
96	0.0000E-39
97	0.0000E-39
98	0.0000E-39
99	0.0000E-39
100	0.0000E-39
101	0.0000E-39
102	0.0000E-39
103	0.0000E-39
104	0.0000E-39
105	0.0000E-39
106	0.0000E-39
107	0.0000E-39
108	0.0000E-39
109	0.0000E-39
110	0.0000E-39
111	0.0000E-39
112	0.0000E-39
113	0.0000E-39

114	0.0000E-39
115	0.0000E-39
116	0.0000E-39
117	0.0000E-39
118	0.0000E-39
119	0.0000E-39
120	0.0000E-39

ea

DEFLECTIONS AND INTERNAL LOADS, TIME = 1.0000E-04

I	U(I)	V(I)	W(I)	M(PHI)	M(THETA)	M(PHI, THETA)	Q(PHI)	Q(THETA)
1	1.8190E-11	-0.0000E-39	5.3015E-03	1.1000E 03	1.1000E 03	0.0000E-39	-7.2222E 00	0.0000E-39
2	-8.0499E-06	-0.0000E-39	5.2702E-03	1.0964E 03	1.0964E 03	-0.0000E-39	-1.4364E 01	-0.0000E-39
3	-1.5960E-05	-0.0000E-39	5.1762E-03	1.0855E 03	1.0906E 03	-0.0000E-39	-3.8050E 01	-0.0000E-39
4	-2.3562E-05	-0.0000E-39	5.0203E-03	1.0631E 03	1.0779E 03	-0.0000E-39	-7.1309E 01	-0.0000E-39
5	-3.0691E-05	-0.0000E-39	4.8041E-03	1.0237E 03	1.0559E 03	-0.0000E-39	-1.2077E 02	-0.0000E-39
6	-3.7186E-05	-0.0000E-39	4.5203E-03	9.5775E 02	1.0201E 02	-0.0000E-39	-1.9893E 02	-0.0000E-39
7	-4.2884E-05	-0.0000E-39	4.2036E-03	8.4849E 02	9.6270E 02	-0.0000E-39	-3.3701E 02	-0.0000E-39
8	-4.7617E-05	-0.0000E-39	3.8315E-03	6.5679E 02	8.6629E 02	-0.0000E-39	-5.9933E 02	-0.0000E-39
9	-5.1203E-05	-0.0000E-39	3.4279E-03	3.0543E 02	6.9702E 02	-0.0000E-39	-6.9143E 02	-0.0000E-39
10	-5.3593E-05	-0.0000E-39	3.0178E-03	5.9116E 01	5.4691E 02	-0.0000E-39	-5.2245E 02	-0.0000E-39
11	-5.4908E-05	-0.0000E-39	2.6180E-03	-1.1177E 02	4.1918E 02	-0.0000E-39	-3.8996E 02	-0.0000E-39
12	-5.5281E-05	-0.0000E-39	2.2395E-03	-2.2702E 02	3.1329E 02	-0.0000E-39	-2.8538E 02	-0.0000E-39
13	-5.4847E-05	-0.0000E-39	1.8893E-03	-3.0065E 02	2.2721E 02	-0.0000E-39	-2.0279E 02	-0.0000E-39
14	-5.3740E-05	-0.0000E-39	1.5710E-03	-3.4307E 02	1.5844E 02	-0.0000E-39	-1.3782E 02	-0.0000E-39
15	-5.2088E-05	-0.0000E-39	1.2865E-03	-3.6218E 02	1.0444E 02	-0.0000E-39	-8.7141E 01	-0.0000E-39
16	-5.0009E-05	0.0000E-39	1.0358E-03	-3.6411E 02	6.2826E 01	-0.0000E-39	-4.8082E 01	-0.0000E-39
17	-4.7610E-05	0.0000E-39	8.1788E-04	-3.5366E 02	3.1438E 01	-0.0000E-39	-1.8488E 01	-0.0000E-39
18	-4.4986E-05	0.0000E-39	6.3103E-04	-3.3460E 02	8.3856E 00	-0.0000E-39	3.4213E 00	-0.0000E-39
19	-4.2220E-05	0.0000E-39	4.7296E-04	-3.0990E 02	-7.9633E 00	-0.0000E-39	1.9127E 01	-0.0000E-39
20	-3.9383E-05	0.0000E-39	3.4108E-04	-2.8184E 02	-1.9001E 01	-0.0000E-39	2.9865E 01	-0.0000E-39
21	-3.6535E-05	0.0000E-39	2.3272E-04	-2.5221E 02	-2.5897E 01	-0.0000E-39	3.6671E 01	-0.0000E-39
22	-3.3724E-05	0.0000E-39	1.4513E-04	-2.2235E 02	-2.9627E 01	-0.0000E-39	4.0407E 01	-0.0000E-39
23	-3.0990E-05	0.0000E-39	7.5680E-05	-1.9323E 02	-3.0992E 01	-0.0000E-39	4.1791E 01	-0.0000E-39
24	-2.8362E-05	0.0000E-39	2.1838E-05	-1.6558E 02	-3.0641E 01	-0.0000E-39	4.1416E 01	-0.0000E-39
25	-2.5863E-05	0.0000E-39	-1.8742E-05	-1.3985E 02	-2.9098E 01	-0.0000E-39	3.9767E 01	-0.0000E-39
26	-2.3508E-05	0.0000E-39	-4.8210E-05	-1.1636E 02	-2.6776E 01	-0.0000E-39	3.7238E 01	-0.0000E-39
27	-2.1308E-05	0.0000E-39	-6.8504E-05	-9.5238E 01	-2.3996E 01	-0.0000E-39	3.4145E 01	-0.0000E-39
28	-1.9267E-05	0.0000E-39	-8.1347E-05	-7.6538E 01	-2.1001E 01	-0.0000E-39	3.0736E 01	-0.0000E-39
29	-1.7386E-05	0.0000E-39	-8.8250E-05	-6.0213E 01	-1.7974E 01	-0.0000E-39	2.7205E 01	-0.0000E-39
30	-1.5662E-05	0.0000E-39	-9.0520E-05	-4.6160E 01	-1.5044E 01	-0.0000E-39	2.3697E 01	-0.0000E-39
31	-1.4092E-05	-0.0000E-39	-8.9272E-05	-3.4233E 01	-1.2302E 01	0.0000E-39	2.0319E 01	0.0000E-39
32	-1.2668E-05	-0.0000E-39	-8.5448E-05	-2.4261E 01	-9.8018E 00	0.0000E-39	1.7146E 01	0.0000E-39
33	-1.1383E-05	-0.0000E-39	-7.9828E-05	-1.6055E 01	-7.5761E 00	0.0000E-39	1.4227E 01	0.0000E-39
34	-1.0227E-05	-0.0000E-39	-7.3048E-05	-9.4207E 00	-5.6365E 00	0.0000E-39	1.1590E 01	0.0000E-39
35	-9.1911E-06	-0.0000E-39	-6.5620E-05	-4.1669E 00	-3.9806E 00	0.0000E-39	9.2473E 00	0.0000E-39
36	-8.2654E-06	-0.0000E-39	-5.7946E-05	-1.0726E-01	-2.5960E 00	0.0000E-39	7.1989E 00	0.0000E-39
37	-7.4403E-06	-0.0000E-39	-5.0334E-05	2.9333E 00	-1.4633E 00	0.0000E-39	5.4351E 00	0.0000E-39
38	-6.7063E-06	-0.0000E-39	-4.3011E-05	5.1170E 00	-5.5916E-01	0.0000E-39	3.9401E 00	0.0000E-39
39	-6.0544E-06	-0.0000E-39	-3.6138E-05	6.5913E 00	1.4222E-01	0.0000E-39	2.6935E 00	0.0000E-39

40	-5.4759E-06	-0.0000E-39	-2.9821E-05	7.4885E 00	6.6718E-01	0.0000E-39	1.6723E 00	0.0000E-39
41	-4.9629E-06	-0.0000E-39	-2.4122E-05	7.9252E 00	1.0416E 00	0.0000E-39	8.5224E-01	0.0000E-39
42	-4.5080E-06	-0.0000E-39	-1.9068E-05	8.0031E 00	1.2900E 00	0.0000E-39	2.0894E-01	0.0000E-39
43	-4.1042E-06	-0.0000E-39	-1.4659E-05	7.8094E 00	1.4353E 00	0.0000E-39	-2.8146E-01	0.0000E-39
44	-3.7455E-06	-0.0000E-39	-1.0874E-05	7.4179E 00	1.4979E 00	0.0000E-39	-6.4160E-01	0.0000E-39
45	-3.4264E-06	-0.0000E-39	-7.6786E-06	6.8900E 00	1.4960E 00	0.0000E-39	-8.9251E-01	0.0000E-39
46	-3.1418E-06	-0.0000E-39	-5.0277E-06	6.2762E 00	1.4457E 00	0.0000E-39	-1.0534E 00	0.0000E-39
47	-2.8873E-06	-0.0000E-39	-2.8705E-06	5.6168E 00	1.3604E 00	0.0000E-39	-1.1415E 00	0.0000E-39
48	-2.6591E-06	-0.0000E-39	-1.1532E-06	4.9438E 00	1.2514E 00	0.0000E-39	-1.1721E 00	0.0000E-39
49	-2.4538E-06	-0.0000E-39	1.7846E-07	4.2815E 00	1.1283E 00	0.0000E-39	-1.1584E 00	0.0000E-39
50	-2.2684E-06	-0.0000E-39	1.1774E-06	3.6479E 00	9.9833E-01	0.0000E-39	-1.1117E 00	0.0000E-39
51	-2.1005E-06	-0.0000E-39	1.8938E-06	3.0557E 00	8.6752E-01	0.0000E-39	-1.0416E 00	0.0000E-39
52	-1.9477E-06	-0.0000E-39	2.3746E-06	2.5132E 00	7.4032E-01	0.0000E-39	-9.5608E-01	0.0000E-39
53	-1.8081E-06	-0.0000E-39	2.6624E-06	2.0249E 00	6.1996E-01	0.0000E-39	-8.6153E-01	0.0000E-39
54	-1.6803E-06	-0.0000E-39	2.7954E-06	1.5928E 00	5.0868E-01	0.0000E-39	-7.6313E-01	0.0000E-39
55	-1.5628E-06	0.0000E-39	2.8072E-06	1.2166E 00	4.0788E-01	-0.0000E-39	-6.6488E-01	-0.0000E-39
56	-1.4543E-06	0.0000E-39	2.7271E-06	8.9428E-01	3.1825E-01	-0.0000E-39	-5.6981E-01	-0.0000E-39
57	-1.3541E-06	0.0000E-39	2.5800E-06	6.2264E-01	2.3999E-01	-0.0000E-39	-4.8009E-01	-0.0000E-39
58	-1.2611E-06	0.0000E-39	2.3869E-06	3.9777E-01	1.7285E-01	-0.0000E-39	-3.9722E-01	-0.0000E-39
59	-1.1747E-06	0.0000E-39	2.1649E-06	2.1523E-01	1.1631E-01	-0.0000E-39	-3.2209E-01	-0.0000E-39
60	-1.0942E-06	0.0000E-39	1.9282E-06	7.0370E-02	6.9603E-02	-0.0000E-39	-2.5516E-01	-0.0000E-39
61	-1.0193E-06	0.0000E-39	1.6876E-06	-4.1482E-02	3.1866E-02	-0.0000E-39	-1.9651E-01	-0.0000E-39
62	-9.4931E-07	0.0000E-39	1.4516E-06	-1.2489E-01	2.1385E-03	-0.0000E-39	-1.4594E-01	-0.0000E-39
63	-8.8397E-07	0.0000E-39	1.2265E-06	-1.8418E-01	-2.0557E-02	-0.0000E-39	-1.0307E-01	-0.0000E-39
64	-8.2292E-07	0.0000E-39	1.0168E-06	-2.2336E-01	-3.7189E-02	-0.0000E-39	-6.7364E-02	-0.0000E-39
65	-7.6587E-07	0.0000E-39	8.2520E-07	-2.4610E-01	-4.8684E-02	-0.0000E-39	-3.8185E-02	-0.0000E-39
66	-7.1254E-07	0.0000E-39	6.5339E-07	-2.5567E-01	-5.5908E-02	-0.0000E-39	-1.4859E-02	-0.0000E-39
67	-6.6270E-07	0.0000E-39	5.0194E-07	-2.5497E-01	-5.9655E-02	-0.0000E-39	3.3048E-03	-0.0000E-39
68	-6.1615E-07	0.0000E-39	3.7070E-07	-2.4650E-01	-6.0637E-02	-0.0000E-39	1.6992E-02	-0.0000E-39
69	-5.7267E-07	0.0000E-39	2.5890E-07	-2.3240E-01	-5.9485E-02	-0.0000E-39	2.6859E-02	-0.0000E-39
70	-5.3209E-07	0.0000E-39	1.6535E-07	-2.1446E-01	-5.6742E-02	-0.0000E-39	3.3522E-02	-0.0000E-39
71	-4.9423E-07	0.0000E-39	8.8607E-08	-1.9416E-01	-5.2875E-02	-0.0000E-39	3.7547E-02	-0.0000E-39
72	-4.5894E-07	0.0000E-39	2.7034E-08	-1.7270E-01	-4.8272E-02	-0.0000E-39	3.9444E-02	-0.0000E-39
73	-4.2605E-07	0.0000E-39	-2.1075E-08	-1.5103E-01	-4.3252E-02	-0.0000E-39	3.9666E-02	-0.0000E-39
74	-3.9543E-07	0.0000E-39	-5.7433E-08	-1.2985E-01	-3.8072E-02	-0.0000E-39	3.8609E-02	-0.0000E-39
75	-3.6694E-07	0.0000E-39	-8.3707E-08	-1.0971E-01	-3.2930E-02	-0.0000E-39	3.6612E-02	-0.0000E-39
76	-3.4044E-07	0.0000E-39	-1.0147E-07	-9.0975E-02	-2.7978E-02	-0.0000E-39	3.3962E-02	-0.0000E-39
77	-3.1580E-07	0.0000E-39	-1.1220E-07	-7.3890E-02	-2.3326E-02	-0.0000E-39	3.0897E-02	-0.0000E-39
78	-2.9291E-07	0.0000E-39	-1.1721E-07	-5.8584E-02	-1.9046E-02	-0.0000E-39	2.7611E-02	-0.0000E-39
79	-2.7166E-07	-0.0000E-39	-1.1770E-07	-4.5104E-02	-1.5184E-02	0.0000E-39	2.4258E-02	0.0000E-39
80	-2.5193E-07	-0.0000E-39	-1.1472E-07	-3.3427E-02	-1.1760E-02	0.0000E-39	2.0956E-02	0.0000E-39
81	-2.3362E-07	-0.0000E-39	-1.0916E-07	-2.3483E-02	-8.7766E-03	0.0000E-39	1.7796E-02	0.0000E-39
82	-2.1662E-07	-0.0000E-39	-1.0179E-07	-1.5164E-02	-6.2223E-03	0.0000E-39	1.4840E-02	0.0000E-39

83	-2.0087E-07	-0.0000E-39	-9.3265E-08	-8.3379E-03	-4.0747E-03	0.0000E-39	1.2130E-02	0.0000E-39
84	-1.8626E-07	-0.0000E-39	-8.4096E-08	-2.8596E-03	-2.3041E-03	0.0000E-39	9.6903E-03	0.0000E-39
85	-1.7270E-07	-0.0000E-39	-7.4707E-08	1.4234E-03	-8.7614E-04	0.0000E-39	7.5318E-03	0.0000E-39
86	-1.6013E-07	-0.0000E-39	-6.5427E-08	4.6635E-03	2.4586E-04	0.0000E-39	5.6535E-03	0.0000E-39
87	-1.4846E-07	-0.0000E-39	-5.6503E-08	7.0088E-03	1.0994E-03	0.0000E-39	4.0462E-03	0.0000E-39
88	-1.3764E-07	-0.0000E-39	-4.8113E-08	8.5993E-03	1.7214E-03	0.0000E-39	2.6947E-03	0.0000E-39
89	-1.2759E-07	-0.0000E-39	-4.0378E-08	9.5648E-03	2.1471E-03	0.0000E-39	1.5794E-03	0.0000E-39
90	-1.1827E-07	-0.0000E-39	-3.3370E-08	1.0023E-02	2.4096E-03	0.0000E-39	6.7837E-04	0.0000E-39
91	-1.0961E-07	-0.0000E-39	-2.7124E-08	1.0080E-02	2.5391E-03	0.0000E-39	-3.1766E-05	0.0000E-39
92	-1.0156E-07	-0.0000E-39	-2.1641E-08	9.8273E-03	2.5627E-03	0.0000E-39	-5.7462E-04	0.0000E-39
93	-9.4075E-08	-0.0000E-39	-1.6902E-08	9.3457E-03	2.5044E-03	0.0000E-39	-9.7332E-04	0.0000E-39
94	-8.7114E-08	-0.0000E-39	-1.2869E-08	8.7029E-03	2.3850E-03	0.0000E-39	-1.2499E-03	0.0000E-39
95	-8.0634E-08	-0.0000E-39	-9.4914E-09	7.9558E-03	2.2225E-03	0.0000E-39	-1.4248E-03	0.0000E-39
96	-7.4596E-08	-0.0000E-39	-6.7116E-09	7.1506E-03	2.0316E-03	0.0000E-39	-1.5168E-03	0.0000E-39
97	-6.8967E-08	-0.0000E-39	-4.4676E-09	6.3248E-03	1.8246E-03	0.0000E-39	-1.5427E-03	0.0000E-39
98	-6.3714E-08	-0.0000E-39	-2.6959E-09	5.5073E-03	1.6114E-03	0.0000E-39	-1.5174E-03	0.0000E-39
99	-5.8806E-08	-0.0000E-39	-1.3339E-09	4.7201E-03	1.3997E-03	0.0000E-39	-1.4536E-03	0.0000E-39
100	-5.4217E-08	-0.0000E-39	-3.2129E-10	3.9791E-03	1.1953E-03	0.0000E-39	-1.3623E-03	0.0000E-39
101	-4.9920E-08	-0.0000E-39	3.9839E-10	3.2950E-03	1.0027E-03	0.0000E-39	-1.2527E-03	0.0000E-39
102	-4.5892E-08	-0.0000E-39	8.7727E-10	2.6743E-03	8.2455E-04	0.0000E-39	-1.1323E-03	0.0000E-39
103	-4.2110E-08	-0.0000E-39	1.1625E-09	2.1203E-03	6.6282E-04	0.0000E-39	-1.0071E-03	0.0000E-39
104	-3.8555E-08	-0.0000E-39	1.2962E-09	1.6335E-03	5.1840E-04	0.0000E-39	-8.8164E-04	0.0000E-39
105	-3.5207E-08	-0.0000E-39	1.3150E-09	1.2124E-03	3.9152E-04	0.0000E-39	-7.5953E-04	0.0000E-39
106	-3.2049E-08	-0.0000E-39	1.2508E-09	8.5407E-04	2.8189E-04	-0.0000E-39	-6.4320E-04	0.0000E-39
107	-2.9063E-08	-0.0000E-39	1.1306E-09	5.5474E-04	1.8884E-04	-0.0000E-39	-5.3428E-04	0.0000E-39
108	-2.6235E-08	0.0000E-39	9.7662E-10	3.0991E-04	1.1145E-04	-0.0000E-39	-4.3365E-04	0.0000E-39
109	-2.3549E-08	0.0000E-39	8.0730E-10	1.1490E-04	4.8674E-05	-0.0000E-39	-3.4163E-04	0.0000E-39
110	-2.0993E-08	0.0000E-39	6.3706E-10	-3.4947E-05	-5.9862E-07	-0.0000E-39	-2.5806E-04	0.0000E-39
111	-1.8553E-08	0.0000E-39	4.7694E-10	-1.4409E-04	-3.7454E-05	-0.0000E-39	-1.8244E-04	0.0000E-39
112	-1.6217E-08	0.0000E-39	3.3489E-10	-2.1660E-04	-6.2907E-05	-0.0000E-39	-1.1399E-04	0.0000E-39
113	-1.3974E-08	0.0000E-39	2.1609E-10	-2.5609E-04	-7.7857E-05	-0.0000E-39	-5.1782E-05	0.0000E-39
114	-1.1813E-08	0.0000E-39	1.2325E-10	-2.6562E-04	-8.3068E-05	-0.0000E-39	5.2256E-06	0.0000E-39
115	-9.7231E-09	0.0000E-39	5.6802E-11	-2.4771E-04	-7.9147E-05	-0.0000E-39	5.8093E-05	0.0000E-39
116	-7.6941E-09	0.0000E-39	1.5148E-11	-2.0433E-04	-6.6547E-05	-0.0000E-39	1.0785E-04	0.0000E-39
117	-5.7166E-09	0.0000E-39	-5.2195E-12	-1.3691E-04	-4.5571E-05	0.0000E-39	1.5543E-04	0.0000E-39
118	-3.7811E-09	-0.0000E-39	-9.5918E-12	-4.6459E-05	-1.6388E-05	0.0000E-39	2.0162E-04	0.0000E-39
119	-1.8785E-09	-0.0000E-39	-4.9673E-12	6.6404E-05	2.0940E-05	0.0000E-39	2.4702E-04	0.0000E-39
120	-0.0000E-39	0.0000E-39	0.0000E-39	2.0130E-04	6.5942E-05	0.0000E-39	2.9227E-04	0.0000E-39

(DR)

I	N(PHI)	N(THETA)	N(PHI,THETA)	SIG(PHI)	SIG(THETA)	SG(PHI,THETA)
1	6.2831E 01	6.2831E 01	0.0000E-39	1.1914E 04	1.1914E 04	0.0000E-39
2	6.2502E 01	6.2193E 01	0.0000E-39	1.1873E 04	1.1870E 04	-0.0000E-39
3	6.1770E 01	6.0775E 01	0.0000E-39	1.1755E 04	1.1796E 04	-0.0000E-39
4	6.0701E 01	5.8535E 01	0.0000E-39	1.1514E 04	1.1644E 04	-0.0000E-39
5	5.9306E 01	5.5490E 01	0.0000E-39	1.1095E 04	1.1388E 04	-0.0000E-39
6	5.7653E 01	5.1709E 01	0.0000E-39	1.0403E 04	1.0983E 04	-0.0000E-39
7	5.5876E 01	4.7311E 01	0.0000E-39	9.2640E 03	1.0350E 04	-0.0000E-39
8	5.4239E 01	4.2520E 01	0.0000E-39	7.2810E 03	9.3130E 03	-0.0000E-39
9	5.2694E 01	3.7562E 01	0.0000E-39	3.6609E 03	7.5267E 03	-0.0000E-39
10	5.0840E 01	3.2650E 01	0.0000E-39	1.1153E 03	5.9376E 03	-0.0000E-39
11	4.8450E 01	2.7844E 01	0.0000E-39	-6.6173E 02	4.5791E 03	-0.0000E-39
12	4.5712E 01	2.3292E 01	0.0000E-39	-1.8714E 03	3.4472E 03	-0.0000E-39
13	4.2769E 01	1.9086E 01	0.0000E-39	-2.6564E 03	2.5220E 03	-0.0000E-39
14	3.9728E 01	1.5282E 01	0.0000E-39	-3.1220E 03	1.7784E 03	-0.0000E-39
15	3.6674E 01	1.1904E 01	0.0000E-39	-3.3486E 03	1.1906E 03	-0.0000E-39
16	3.3669E 01	8.9574E 00	-0.0000E-39	-3.3984E 03	7.3419E 02	0.0000E-39
17	3.0760E 01	6.4294E 00	-0.0000E-39	-3.3204E 03	3.8687E 02	0.0000E-39
18	2.7981E 01	4.2981E 00	-0.0000E-39	-3.1527E 03	1.2905E 02	0.0000E-39
19	2.5355E 01	2.5340E 00	-0.0000E-39	-2.9255E 03	-5.6333E 01	0.0000E-39
20	2.2897E 01	1.1034E 00	-0.0000E-39	-2.6623E 03	-1.8389E 02	0.0000E-39
21	2.0615E 01	-2.9634E-02	-0.0000E-39	-2.3812E 03	-2.6598E 02	0.0000E-39
22	1.8512E 01	-9.0132E-01	-0.0000E-39	-2.0958E 03	-3.1297E 02	0.0000E-39
23	1.6585E 01	-1.5471E 00	-0.0000E-39	-1.8164E 03	-3.3343E 02	0.0000E-39
24	1.4832E 01	-2.0008E 00	-0.0000E-39	-1.5502E 03	-3.3438E 02	0.0000E-39
25	1.3243E 01	-2.2938E 00	-0.0000E-39	-1.3022E 03	-3.2148E 02	0.0000E-39
26	1.1811E 01	-2.4549E 00	-0.0000E-39	-1.0755E 03	-2.9927E 02	0.0000E-39
27	1.0526E 01	-2.5100E 00	-0.0000E-39	-8.7170E 02	-2.7129E 02	0.0000E-39
28	9.3764E 00	-2.4818E 00	-0.0000E-39	-6.9136E 02	-2.4029E 02	0.0000E-39
29	8.3520E 00	-2.3903E 00	-0.0000E-39	-5.3413E 02	-2.0832E 02	0.0000E-39
30	7.4419E 00	-2.2527E 00	-0.0000E-39	-3.9907E 02	-1.7689E 02	0.0000E-39
31	6.6354E 00	-2.0833E 00	0.0000E-39	-2.8479E 02	-1.4706E 02	0.0000E-39
32	5.9223E 00	-1.8941E 00	0.0000E-39	-1.8962E 02	-1.1952E 02	0.0000E-39
33	5.2929E 00	-1.6950E 00	0.0000E-39	-1.1173E 02	-9.4689E 01	0.0000E-39
34	4.7382E 00	-1.4936E 00	0.0000E-39	-4.9224E 01	-7.2775E 01	0.0000E-39
35	4.2498E 00	-1.2962E 00	0.0000E-39	-2.1262E-01	-5.3811E 01	0.0000E-39
36	3.8199E 00	-1.1071E 00	0.0000E-39	3.7133E 01	-3.7714E 01	0.0000E-39
37	3.4415E 00	-9.2981E-01	0.0000E-39	6.4539E 01	-2.4319E 01	0.0000E-39
38	3.1083E 00	-7.6635E-01	0.0000E-39	8.3606E 01	-1.3407E 01	0.0000E-39
39	2.8146E 00	-6.1808E-01	0.0000E-39	9.5792E 01	-4.7273E 00	0.0000E-39
40	2.5553E 00	-4.8557E-01	0.0000E-39	1.0240E 02	1.9846E 00	0.0000E-39
41	2.3259E 00	-3.6884E-01	0.0000E-39	1.0459E 02	6.9941E 00	0.0000E-39
42	2.1221E 00	-2.6747E-01	0.0000E-39	1.0335E 02	1.0558E 01	-0.0000E-39

43	1.9416E 00	-1.8069E-01	0.0000E-39	9.9551E 01	1.2916E 01	-0.0000E-39
44	1.7802E 00	-1.0755E-01	0.0000E-39	9.3919E 01	1.4290E 01	-0.0000E-39
45	1.6358E 00	-4.6917E-02	0.0000E-39	8.7058E 01	1.4878E 01	-0.0000E-39
46	1.5060E 00	2.4225E-03	0.0000E-39	7.9462E 01	1.4856E 01	-0.0000E-39
47	1.3890E 00	4.1701E-02	0.0000E-39	7.1526E 01	1.4374E 01	-0.0000E-39
48	1.2830E 00	7.2146E-02	0.0000E-39	6.3561E 01	1.3561E 01	-0.0000E-39
49	1.1867E 00	9.4940E-02	0.0000E-39	5.5802E 01	1.2525E 01	-0.0000E-39
50	1.0989E 00	1.1120E-01	0.0000E-39	4.8423E 01	1.1355E 01	-0.0000E-39
51	1.0185E 00	1.2197E-01	0.0000E-39	4.1543E 01	1.0121E 01	-0.0000E-39
52	9.4470E-01	1.2819E-01	0.0000E-39	3.5238E 01	8.8780E 00	-0.0000E-39
53	8.7676E-01	1.3071E-01	0.0000E-39	2.9549E 01	7.6685E 00	-0.0000E-39
54	8.1406E-01	1.3028E-01	0.0000E-39	2.4489E 01	6.5226E 00	-0.0000E-39
55	7.5606E-01	1.2757E-01	-0.0000E-39	2.0049E 01	5.4613E 00	-0.0000E-39
56	7.0232E-01	1.2314E-01	-0.0000E-39	1.6204E 01	4.4976E 00	-0.0000E-39
57	6.5244E-01	1.1748E-01	-0.0000E-39	1.2918E 01	3.6380E 00	-0.0000E-39
58	6.0610E-01	1.1099E-01	-0.0000E-39	1.0147E 01	2.8842E 00	-0.0000E-39
59	5.6300E-01	1.0399E-01	-0.0000E-39	7.8431E 00	2.2341E 00	-0.0000E-39
60	5.2291E-01	9.6771E-02	-0.0000E-39	5.9556E 00	1.6826E 00	-0.0000E-39
61	4.8558E-01	8.9528E-02	-0.0000E-39	4.4346E 00	1.2230E 00	-0.0000E-39
62	4.5083E-01	8.2431E-02	-0.0000E-39	3.2311E 00	8.4698E-01	-0.0000E-39
63	4.1849E-01	7.5601E-02	-0.0000E-39	2.2991E 00	5.4578E-01	-0.0000E-39
64	3.8838E-01	6.9124E-02	-0.0000E-39	1.5958E 00	3.1033E-01	-0.0000E-39
65	3.6036E-01	6.3058E-02	-0.0000E-39	1.0820E 00	1.3169E-01	-0.0000E-39
66	3.3429E-01	5.7436E-02	-0.0000E-39	7.2296E-01	1.3065E-03	-0.0000E-39
67	3.1006E-01	5.2272E-02	-0.0000E-39	4.8759E-01	-8.8817E-02	0.0000E-39
68	2.8754E-01	4.7566E-02	-0.0000E-39	3.4906E-01	-1.4601E-01	0.0000E-39
69	2.6661E-01	4.3304E-02	-0.0000E-39	2.8433E-01	-1.7684E-01	0.0000E-39
70	2.4719E-01	3.9467E-02	-0.0000E-39	2.7394E-01	-1.8711E-01	0.0000E-39
71	2.2916E-01	3.6027E-02	-0.0000E-39	3.0173E-01	-1.8186E-01	0.0000E-39
72	2.1244E-01	3.2956E-02	-0.0000E-39	3.5453E-01	-1.6537E-01	0.0000E-39
73	1.9694E-01	3.0221E-02	-0.0000E-39	4.2178E-01	-1.4125E-01	0.0000E-39
74	1.8258E-01	2.7790E-02	-0.0000E-39	4.9526E-01	-1.1243E-01	0.0000E-39
75	1.6927E-01	2.5631E-02	-0.0000E-39	5.6870E-01	-8.1294E-02	0.0000E-39
76	1.5695E-01	2.3713E-02	-0.0000E-39	6.3757E-01	-4.9691E-02	0.0000E-39
77	1.4554E-01	2.2008E-02	-0.0000E-39	6.9868E-01	-1.9029E-02	0.0000E-39
78	1.3499E-01	2.0488E-02	-0.0000E-39	7.5005E-01	9.6664E-03	0.0000E-39
79	1.2522E-01	1.9130E-02	0.0000E-39	7.9058E-01	3.5695E-02	0.0000E-39
80	1.1618E-01	1.7911E-02	0.0000E-39	8.1993E-01	5.8623E-02	0.0000E-39
81	1.0782E-01	1.6812E-02	0.0000E-39	8.3829E-01	7.8231E-02	0.0000E-39
82	1.0009E-01	1.5817E-02	0.0000E-39	8.4625E-01	9.4471E-02	0.0000E-39
83	9.2942E-02	1.4910E-02	0.0000E-39	8.4470E-01	1.0743E-01	0.0000E-39
84	8.6328E-02	1.4079E-02	0.0000E-39	8.3471E-01	1.1728E-01	0.0000E-39
85	8.0211E-02	1.3313E-02	0.0000E-39	8.1742E-01	1.2426E-01	0.0000E-39

86	7.4553E-02	1.2604E-02	0.0000E-39	7.9404E-01	1.2867E-01	0.0000E-39
87	6.9320E-02	1.1943E-02	0.0000E-39	7.6572E-01	1.3082E-01	0.0000E-39
88	6.4479E-02	1.1326E-02	0.0000E-39	7.3358E-01	1.3102E-01	0.0000E-39
89	6.0001E-02	1.0746E-02	0.0000E-39	6.9867E-01	1.2959E-01	0.0000E-39
90	5.5859E-02	1.0201E-02	0.0000E-39	6.6191E-01	1.2682E-01	0.0000E-39
91	5.2027E-02	9.6858E-03	0.0000E-39	6.2414E-01	1.2299E-01	-0.0000E-39
92	4.8483E-02	9.1994E-03	0.0000E-39	5.8608E-01	1.1837E-01	-0.0000E-39
93	4.5204E-02	8.7394E-03	0.0000E-39	5.4832E-01	1.1316E-01	-0.0000E-39
94	4.2172E-02	8.3045E-03	0.0000E-39	5.1138E-01	1.0759E-01	-0.0000E-39
95	3.9368E-02	7.8934E-03	0.0000E-39	4.7565E-01	1.0180E-01	-0.0000E-39
96	3.6776E-02	7.5053E-03	0.0000E-39	4.4145E-01	9.5962E-02	-0.0000E-39
97	3.4381E-02	7.1395E-03	0.0000E-39	4.0901E-01	9.0177E-02	-0.0000E-39
98	3.2169E-02	6.7955E-03	0.0000E-39	3.7848E-01	8.4546E-02	-0.0000E-39
99	3.0127E-02	6.4728E-03	0.0000E-39	3.4996E-01	7.9145E-02	-0.0000E-39
100	2.8243E-02	6.1711E-03	0.0000E-39	3.2350E-01	7.4029E-02	-0.0000E-39
101	2.6507E-02	5.8900E-03	0.0000E-39	2.9911E-01	6.9239E-02	-0.0000E-39
102	2.4909E-02	5.6293E-03	0.0000E-39	2.7674E-01	6.4802E-02	-0.0000E-39
103	2.3439E-02	5.3886E-03	0.0000E-39	2.5635E-01	6.0734E-02	-0.0000E-39
104	2.2090E-02	5.1677E-03	0.0000E-39	2.3785E-01	5.7041E-02	-0.0000E-39
105	2.0854E-02	4.9662E-03	0.0000E-39	2.2116E-01	5.3723E-02	-0.0000E-39
106	1.9724E-02	4.7840E-03	0.0000E-39	2.0618E-01	5.0774E-02	-0.0000E-39
107	1.8694E-02	4.6205E-03	0.0000E-39	1.9279E-01	4.8183E-02	-0.0000E-39
108	1.7758E-02	4.4756E-03	-0.0000E-39	1.8091E-01	4.5939E-02	-0.0000E-39
109	1.6910E-02	4.3490E-03	-0.0000E-39	1.7043E-01	4.4028E-02	-0.0000E-39
110	1.6147E-02	4.2403E-03	-0.0000E-39	1.6126E-01	4.2434E-02	-0.0000E-39
111	1.5464E-02	4.1492E-03	-0.0000E-39	1.5330E-01	4.1145E-02	-0.0000E-39
112	1.4856E-02	4.0756E-03	-0.0000E-39	1.4647E-01	4.0147E-02	-0.0000E-39
113	1.4321E-02	4.0191E-03	-0.0000E-39	1.4071E-01	3.9428E-02	-0.0000E-39
114	1.3856E-02	3.9795E-03	-0.0000E-39	1.3596E-01	3.8978E-02	0.0000E-39
115	1.3457E-02	3.9566E-03	-0.0000E-39	1.3215E-01	3.8789E-02	0.0000E-39
116	1.3122E-02	3.9502E-03	-0.0000E-39	1.2924E-01	3.8854E-02	0.0000E-39
117	1.2849E-02	3.9602E-03	-0.0000E-39	1.2720E-01	3.9169E-02	0.0000E-39
118	1.2637E-02	3.9864E-03	0.0000E-39	1.2600E-01	3.9732E-02	0.0000E-39
119	1.2483E-02	4.0289E-03	0.0000E-39	1.2562E-01	4.0539E-02	0.0000E-39
120	1.2357E-02	4.0779E-03	-0.0000E-39	1.2575E-01	4.1492E-02	0.0000E-39

VELOCITIES AND ACCELERATIONS

EA

VEL (U)	VEL (V)	VEL (W)	ACC (U)	ACC (V)	ACC (W)
.819E-07	-0.000E-39	5.301E 01	1.819E-03	0.000E-39	5.301E 05

-8.050E-02	-0.000E-39	5.270E 01	-8.050E 02	0.000E-39	5.270E 05
-1.596E-01	-0.000E-39	5.176E 01	-1.596E 03	0.000E-39	5.176E 05
-2.356E-01	-0.000E-39	5.020E 01	-2.356E 03	0.000E-39	5.020E 05
-3.069E-01	-0.000E-39	4.804E 01	-3.069E 03	0.000E-39	4.804E 05
-3.719E-01	-0.000E-39	4.530E 01	-3.719E 03	0.000E-39	4.530E 05
-4.288E-01	-0.000E-39	4.204E 01	-4.288E 03	0.000E-39	4.204E 05
-4.762E-01	-0.000E-39	3.832E 01	-4.762E 03	0.000E-39	3.832E 05
-5.120E-01	-0.000E-39	3.428E 01	-5.120E 03	0.000E-39	3.428E 05
-5.359E-01	-0.000E-39	3.018E 01	-5.359E 03	0.000E-39	3.018E 05
-5.491E-01	-0.000E-39	2.618E 01	-5.491E 03	0.000E-39	2.618E 05
-5.528E-01	-0.000E-39	2.240E 01	-5.528E 03	0.000E-39	2.240E 05
-5.485E-01	-0.000E-39	1.889E 01	-5.485E 03	0.000E-39	1.889E 05
-5.374E-01	-0.000E-39	1.571E 01	-5.374E 03	0.000E-39	1.571E 05
-5.209E-01	-0.000E-39	1.286E 01	-5.209E 03	0.000E-39	1.286E 05
-5.001E-01	0.000E-39	1.036E 01	-5.001E 03	0.000E-39	1.036E 05
-4.761E-01	0.000E-39	8.179E 00	-4.761E 03	0.000E-39	8.179E 04
-4.499E-01	0.000E-39	6.310E 00	-4.499E 03	0.000E-39	6.310E 04
-4.222E-01	0.000E-39	4.730E 00	-4.222E 03	0.000E-39	4.730E 04
-3.938E-01	0.000E-39	3.411E 00	-3.938E 03	0.000E-39	3.411E 04
-3.653E-01	0.000E-39	2.327E 00	-3.653E 03	0.000E-39	2.327E 04
-3.372E-01	0.000E-39	1.451E 00	-3.372E 03	0.000E-39	1.451E 04
-3.099E-01	0.000E-39	7.568E-01	-3.099E 03	0.000E-39	7.568E 03
-2.836E-01	0.000E-39	2.184E-01	-2.836E 03	0.000E-39	2.184E 03
-2.586E-01	0.000E-39	-1.874E-01	-2.586E 03	0.000E-39	-1.874E 03
-2.351E-01	0.000E-39	-4.821E-01	-2.351E 03	0.000E-39	-4.821E 03
-2.131E-01	0.000E-39	-6.850E-01	-2.131E 03	0.000E-39	-6.850E 03
-1.927E-01	0.000E-39	-8.135E-01	-1.927E 03	0.000E-39	-8.135E 03
-1.739E-01	0.000E-39	-8.825E-01	-1.739E 03	0.000E-39	-8.825E 03
-1.566E-01	0.000E-39	-9.052E-01	-1.566E 03	0.000E-39	-9.052E 03
-1.409E-01	-0.000E-39	-8.927E-01	-1.409E 03	0.000E-39	-8.927E 03
-1.267E-01	-0.000E-39	-8.545E-01	-1.267E 03	0.000E-39	-8.545E 03
-1.138E-01	-0.000E-39	-7.983E-01	-1.138E 03	0.000E-39	-7.983E 03
-1.023E-01	-0.000E-39	-7.305E-01	-1.023E 03	0.000E-39	-7.305E 03
-9.191E-02	-0.000E-39	-6.562E-01	-9.191E 02	0.000E-39	-6.562E 03
-8.265E-02	-0.000E-39	-5.795E-01	-8.265E 02	0.000E-39	-5.795E 03
-7.440E-02	-0.000E-39	-5.033E-01	-7.440E 02	0.000E-39	-5.033E 03
-6.706E-02	-0.000E-39	-4.301E-01	-6.706E 02	0.000E-39	-4.301E 03
-6.054E-02	-0.000E-39	-3.614E-01	-6.054E 02	0.000E-39	-3.614E 03
-5.476E-02	-0.000E-39	-2.982E-01	-5.476E 02	0.000E-39	-2.982E 03
-4.963E-02	-0.000E-39	-2.412E-01	-4.963E 02	0.000E-39	-2.412E 03
-4.508E-02	-0.000E-39	-1.907E-01	-4.508E 02	0.000E-39	-1.907E 03
-4.104E-02	-0.000E-39	-1.466E-01	-4.104E 02	0.000E-39	-1.466E 03
-3.746E-02	-0.000E-39	-1.087E-01	-3.746E 02	0.000E-39	-1.087E 03

-1.376E-03	-0.000E-39	-4.811E-04	-1.376E 01	0.000E-39	-4.811E 00
-1.276E-03	-0.000E-39	-4.038E-04	-1.276E 01	0.000E-39	-4.038E 00
-1.183E-03	-0.000E-39	-3.337E-04	-1.183E 01	0.000E-39	-3.337E 00
-1.096E-03	-0.000E-39	-2.712E-04	-1.096E 01	0.000E-39	-2.712E 00
-1.016E-03	-0.000E-39	-2.164E-04	-1.016E 01	0.000E-39	-2.164E 00
-9.408E-04	-0.000E-39	-1.690E-04	-9.408E 00	0.000E-39	-1.690E 00
-8.711E-04	-0.000E-39	-1.287E-04	-8.711E 00	0.000E-39	-1.287E 00
-8.063E-04	-0.000E-39	-9.491E-05	-8.063E 00	0.000E-39	-9.491E-01
-7.460E-04	-0.000E-39	-6.712E-05	-7.460E 00	0.000E-39	-6.712E-01
-6.897E-04	-0.000E-39	-4.468E-05	-6.897E 00	0.000E-39	-4.468E-01
-6.371E-04	-0.000E-39	-2.696E-05	-6.371E 00	0.000E-39	-2.696E-01
-5.881E-04	-0.000E-39	-1.334E-05	-5.881E 00	0.000E-39	-1.334E-01
-5.422E-04	-0.000E-39	-3.213E-06	-5.422E 00	0.000E-39	-3.213E-02
-4.992E-04	-0.000E-39	3.984E-06	-4.992E 00	0.000E-39	3.984E-02
-4.589E-04	-0.000E-39	8.773E-06	-4.589E 00	0.000E-39	8.773E-02
-4.211E-04	-0.000E-39	1.163E-05	-4.211E 00	0.000E-39	1.163E-01
-3.856E-04	-0.000E-39	1.296E-05	-3.856E 00	0.000E-39	1.296E-01
-3.521E-04	-0.000E-39	1.315E-05	-3.521E 00	0.000E-39	1.315E-01
-3.205E-04	-0.000E-39	1.251E-05	-3.205E 00	0.000E-39	1.251E-01
-2.906E-04	-0.000E-39	1.131E-05	-2.906E 00	0.000E-39	1.131E-01
-2.623E-04	0.000E-39	9.766E-06	-2.623E 00	0.000E-39	9.766E-02
-2.355E-04	0.000E-39	8.073E-06	-2.355E 00	0.000E-39	8.073E-02
-2.099E-04	0.000E-39	6.371E-06	-2.099E 00	0.000E-39	6.371E-02
-1.855E-04	0.000E-39	4.769E-06	-1.855E 00	0.000E-39	4.769E-02
-1.622E-04	0.000E-39	3.349E-06	-1.622E 00	0.000E-39	3.349E-02
-1.397E-04	0.000E-39	2.161E-06	-1.397E 00	0.000E-39	2.161E-02
-1.181E-04	0.000E-39	1.232E-06	-1.181E 00	0.000E-39	1.232E-02
-9.723E-05	0.000E-39	5.680E-07	-9.723E-01	0.000E-39	5.680E-03
-7.694E-05	0.000E-39	1.515E-07	-7.694E-01	0.000E-39	1.515E-03
-5.717E-05	0.000E-39	-5.220E-08	-5.717E-01	0.000E-39	-5.220E-04
-3.781E-05	-0.000E-39	-9.592E-08	-3.781E-01	0.000E-39	-9.592E-04
-1.879E-05	-0.000E-39	-4.967E-08	-1.879E-01	0.000E-39	-4.967E-04
-0.000E-39	0.000E-39	0.000E-39	-0.000E-39	0.000E-39	0.000E-39

-3.426E-02	-0.000E-39	-7.679E-02	-3.426E 02	0.000E-39	-7.679E 02
-3.142E-02	-0.000E-39	-5.028E-02	-3.142E 02	0.000E-39	-5.028E 02
-2.887E-02	-0.000E-39	-2.870E-02	-2.887E 02	0.000E-39	-2.870E 02
-2.659E-02	-0.000E-39	-1.153E-02	-2.659E 02	0.000E-39	-1.153E 02
-2.454E-02	-0.000E-39	1.785E-03	-2.454E 02	0.000E-39	1.785E 01
-2.268E-02	-0.000E-39	1.177E-02	-2.268E 02	0.000E-39	1.177E 02
-2.100E-02	-0.000E-39	1.894E-02	-2.100E 02	0.000E-39	1.894E 02
-1.948E-02	-0.000E-39	2.375E-02	-1.948E 02	0.000E-39	2.375E 02
-1.808E-02	-0.000E-39	2.662E-02	-1.808E 02	0.000E-39	2.662E 02
-1.680E-02	-0.000E-39	2.795E-02	-1.680E 02	0.000E-39	2.795E 02
-1.563E-02	0.000E-39	2.807E-02	-1.563E 02	0.000E-39	2.807E 02
-1.454E-02	0.000E-39	2.727E-02	-1.454E 02	0.000E-39	2.727E 02
-1.354E-02	0.000E-39	2.580E-02	-1.354E 02	0.000E-39	2.580E 02
-1.261E-02	0.000E-39	2.387E-02	-1.261E 02	0.000E-39	2.387E 02
-1.175E-02	0.000E-39	2.165E-02	-1.175E 02	0.000E-39	2.165E 02
-1.094E-02	0.000E-39	1.928E-02	-1.094E 02	0.000E-39	1.928E 02
-1.019E-02	0.000E-39	1.688E-02	-1.019E 02	0.000E-39	1.688E 02
-9.493E-03	0.000E-39	1.452E-02	-9.493E 01	0.000E-39	1.452E 02
-8.840E-03	0.000E-39	1.227E-02	-8.840E 01	0.000E-39	1.227E 02
-8.229E-03	0.000E-39	1.017E-02	-8.229E 01	0.000E-39	1.017E 02
-7.659E-03	0.000E-39	8.252E-03	-7.659E 01	0.000E-39	8.252E 01
-7.125E-03	0.000E-39	6.534E-03	-7.125E 01	0.000E-39	6.534E 01
-6.627E-03	0.000E-39	5.019E-03	-6.627E 01	0.000E-39	5.019E 01
-6.161E-03	0.000E-39	3.707E-03	-6.161E 01	0.000E-39	3.707E 01
-5.727E-03	0.000E-39	2.589E-03	-5.727E 01	0.000E-39	2.589E 01
-5.321E-03	0.000E-39	1.654E-03	-5.321E 01	0.000E-39	1.654E 01
-4.942E-03	0.000E-39	8.861E-04	-4.942E 01	0.000E-39	8.861E 00
-4.589E-03	0.000E-39	2.703E-04	-4.589E 01	0.000E-39	2.703E 00
-4.261E-03	0.000E-39	-2.107E-04	-4.261E 01	0.000E-39	-2.107E 00
-3.954E-03	0.000E-39	-5.743E-04	-3.954E 01	0.000E-39	-5.743E 00
-3.669E-03	0.000E-39	-8.371E-04	-3.669E 01	0.000E-39	-8.371E 00
-3.404E-03	0.000E-39	-1.015E-03	-3.404E 01	0.000E-39	-1.015E 01
-3.158E-03	0.000E-39	-1.122E-03	-3.158E 01	0.000E-39	-1.122E 01
-2.929E-03	0.000E-39	-1.172E-03	-2.929E 01	0.000E-39	-1.172E 01
-2.717E-03	-0.000E-39	-1.177E-03	-2.717E 01	0.000E-39	-1.177E 01
-2.519E-03	-0.000E-39	-1.147E-03	-2.519E 01	0.000E-39	-1.147E 01
-2.336E-03	-0.000E-39	-1.092E-03	-2.336E 01	0.000E-39	-1.092E 01
-2.166E-03	-0.000E-39	-1.018E-03	-2.166E 01	0.000E-39	-1.018E 01
-2.009E-03	-0.000E-39	-9.327E-04	-2.009E 01	0.000E-39	-9.327E 00
-1.863E-03	-0.000E-39	-8.410E-04	-1.863E 01	0.000E-39	-8.410E 00
-1.727E-03	-0.000E-39	-7.471E-04	-1.727E 01	0.000E-39	-7.471E 00
-1.601E-03	-0.000E-39	-6.543E-04	-1.601E 01	0.000E-39	-6.543E 00
-1.485E-03	-0.000E-39	-5.650E-04	-1.485E 01	0.000E-39	-5.650E 00

7.1 PROC

6.1 WARNINGS AND RECOMMENDATIONS

6.1.1 Choice of Time Interval

The proper choice of the appropriate time interval Δt is important for obtaining good results. If Δt is too large, the response will be highly damped and inaccurate. On the other hand, if Δt is too small, the program will take a large amount of time to run. In the sample problem Δt of 0.05 ms was used, which gave good results.

6.1.2 Number of Iterations

There is an unidentifiable bug in the problem which makes it necessary that a restart be made after about 140 iterations through the shell program. Should 160 iterations be exceeded, the program will "blow up." Therefore, it is recommended that the job be run in segments of roughly 120 iterations between restarts. The method of restarting is explained in Sections 1.3 and 5.3.

6.1.3 DECRD

The subroutine DECRD is in the NAA program library and consequently does not appear specifically in the source decks. In installations without this program in their library, the subroutine should be inserted in the zero link behind the subroutine MMY.

7.1 PROGRAM LISTING

C	PNCH	NON-ZERO, PUNCH CARDS FOR POSSIBLE RESTART	00000380
C	R(I)	DISTANCE FROM AXIS (IN) COMPUTED BY SUBR. GEOM	00000390
C	WTHD(I)	NON-DIMENSIONAL CURVATURE - THETA DIRECTION	00000400
C	WFE(I)	DITTO * * * - PHI DIRECTION	00000410
C	GAMA(I)	RHO' / RHOX	00000420
C	RPOX(I)	R / AO	00000430
C	D(I)	MEMBRANE STIFFNESS (DIMENSIONLESS)	00000440
C	EK(I)	BENDING STIFFNESS (DIM)	00000450
C	E1(I)	MODULUS OF ELASTICITY	00000460
C	ALF(I)	THERMAL EXPANSION COEFFICIENT	00000470
C	DNA(I)	DISTANCE FROM NEUTRAL AXIS	00000480
C	T(I)	TEMPERATURE CHANGE	00000490
C	ENT(I)	TEMPERATURE LOAD (DIM)	00000500
C	EMT(I)	TEMPERATURE LOAD (DIM)	00000510
C	PFE(I)	FOURIER COMPONENT FOR LOAD - PHI DIRECTION	00000520
C	PTH(I)	DITTO * * *	00000530
C	PN(I)	DITTO * * *	00000540
C	DZ0,VZ0,AZ0	COEF. OF INITIAL VALUES OF DISPLACEMENT, VELOCITY, LD.	00000550
C	DF0,VF0,AF0	** DITTO **	00000560
C	EM1(4,4)	DIAGONAL BOUNDARY FORCE MATRIX (OMEGA)	00000570
C	EM3(4,4)	DIAGONAL BOUNDARY DISPLACEMENT MATRIX (LAMBDA)	00000580
C	EM5(4)	COLUMN BOUNDARY MATRIX (L)	00000590
C	EMIN(4,4)	DIAGONAL BOUNDARY FORCE MATRIX AT BOTTOM	00000600
C	EM3N(4,4)	DIAGONAL BOUNDARY DISPLACEMENT MATRIX AT BOTTOM	00000610
C	EM5N(4)	COLUMN BOUNDARY MATRIX AT BOTTOM	00000620
C	MO(I)	MASS PER UNIT AREA OF SHELL = 2.*DNA(I) * MASS	00000630
C	TDEL	TIME INCREMENT, CURRENT. E.G. TAU1 / ENT1	00000640
C	NJT	NUMBER OF TIME INCREMENTS DESIRED, CURRENT	00000650
C	TIME	RUNNING TIME COUNT	00000660
C	PRNT	CURRENT PRINT INTERVAL	00000670
C			00000680
C			00000690
C			00000700
C			00000710
C			00000720
C			00000730
C			00000740

* * * PARAMETERS PRECEDED BY * ARE READ IN EXECUTIVE PROGRAM, OTHERS ARE SET IN GEOM OR CRVFIT.

DIMENSION BCD(36), PN(200)

C

REAL	MASS, LM11, LM22, LM33, NM11, NM22, MM33, NM11, NM22, NM33,	00000750
1	MO	00000760
EQUIVALENCE	(DA(1), EN), (DA(2), AO), (DA(3), HO),	00000770
1(DA(4), EO), (DA(5), SIGO), (DA(6), ENFO), (DA(7), ENFL),		00000780
2(DA(8), POI), (DA(9), THETA), (DA(10), PIXI), (DA(11), SPRL),		00000790
3(DA(12), UK), (DA(13), VK), (DA(14), WK), (DA(15), EMK),		00000800
4(DA(16), TAU1), (DA(17), ENY1), (DA(18), P11), (DA(19), TAU2),		00000810
5(DA(20), ENT2), (DA(21), P12), (DA(22), TAU3), (DA(23), ENT3),		00000820
6(DA(24), P13), (DA(25), MASS), (DA(26), CFE), (DA(27), CZ),		00000830
7(DA(28), SKFE), (DA(29), SKZ), (DA(30), SUM), (DA(31), EN1),		00000840
8(DA(32), DEL), (DA(33), TFI), (DA(34), VIN), (DA(35), RHO),		00000850
9(DA(36), RESTR1), (DA(37), PNCH), (DA(39), DRW),		00000860
EQUIVALENCE	(DA(40), R), (DA(240), WTHD), (DA(440), WFE),	00000870
1(DA(640), GAMA), (DA(840), RHGX), (DA(1040), D), (DA(1240), EK),		00000880
2(DA(1440), EI), (DA(1640), ALF), (DA(1840), DNA), (DA(2040), T),		00000890
3(DA(2240), ENT), (DA(2440), EMT), (DA(2640), PN), (DA(2840), PFE),		00000900
4(DA(3040), PTH), (DA(3240), DZO), (DA(3440), VZO), (DA(3640), AZO),		00000910
5(DA(3840), DFO), (DA(4040), VFO), (DA(4240), AFO), (DA(4440), EMI),		00000920
6(DA(4456), EM3), (DA(4472), EM5), (DA(4476), EMIN), (DA(4492), EM3N),		00000930
7(DA(4508), EM5N)		00000940
		00000950
		00000960
COMMON	DA(4511), EM2(4,4), EM4(4,4), EM6(4,4), S1, S2, ELAM2,	00000970
1	Z(4,200), X(4,200), A2(4,4), B2(4,4), C2(4,4), G2(4,4), E(4,4),	00000980
2	F(4,4), GA(4,4), A(4,4), B(4,4), C(4,4), G(4,4), EC(4,4), DEL2,	00000990
3	SL1, SL2, N, NTH, NTPR, NTPW, I, K, L,	00001000
4	S77, S78, BTall, BTA33, MO(200), DMG2(200), ZP(3,200),	00001010
5	Z2P(3,200), Z3P(3,200), TIMX, TDEL, PRNT, ENF, PRI, JT, NJT, WT	00001020
		00001030
		00001040
		00001050
		00001060
		00001070
		00001080
		00001090
		00001100
		00001110

C

C

ZERO DATA AND SELECTED MATRICES

1	DO	2	I = 1,4511
2	DA(1)	=	0.
DO	4	K = 1,3	
DO	4	L = 1,200	
ZP(K,L)	=	0.	
Z2P(K,L)	=	0.	
Z3P(K,L)	=	0.	

	READ AND PRINT TITLE CARDS	
C	5 READ	00001120
	6 FORMAT(12A6)	00001130
	WRITE	00001140
	(6, 7) BCD	00001150
	7 FORMAT(1H1 / (18X, 12A6 //))	00001160
C	WT = WEIGHT OF BODY, LBS.	00001170
C	RHO = FLUID DENSITY, LBS/CU FT	00001180
C	VIN=INITIAL IMPACT VELOCITY, FT/SEC	00001190
	READ(5,100) VIN,RHO,WT	00001200
	100 FORMAT(3E12.8)	
	RHO=RHO/1728.	00001210
	VIN=VIN*12.	00001230
	SL2 = 1.	00001240
	NTPW = 9	00001250
	NTPR = 10	00001260
	10 JIMX = 0.	00001270
	JT = 1	00001280
	REWIND NTPW	00001290
	REWIND NTPR	00001300
C	12 CALL DECRD(DA)	00001310
C		00001320
	TDEL = TAUI / ENT1	00001330
	PRNT = PI1	00001340
	ENF = ENFO	00001350
	NJT = ENT1	00001360
	PRI = PI1	00001370
	NTH = 0	00001380
	ELAM = HO / AO	00001390
	ELAM2 = ELAM **2	00001400
	S1 = 1. - POI	00001410
	S2 = 1. + POI	00001420
	S77 = AO/EO * AC/HO	00001430
C		00001440
C		00001450
	GEOMETRY	00001460
		00001470
C	20 CALL GEOM	00001480

```

25 S78 = 2. * DEL /TDEL
REWIND 8
TIMX = TIMX + TDEL
IF(TFI .GE. 0.) GO TO 30
IF(TIMX .NE. TDEL) GO TO 32
V1 = VIN
C
30 CALL CRVFIT
C
COLUMN DATA SET-UP
NORMAL PRESSURES
C
IF(TFI .GE. 0.) GO TO 40
32 CALL ACCN (PMAX, RMAX)
WRITE( 6,33) RMAX,
33 FORMAT(1H1/// 37X, 33HLOADS OUTPUT FROM ACCN SUBROUTINE /// 26X,
1 31HMAX RAD. OF PRESSURE PROFILE =, 1PE12.4/
2 50X, 7HTIME =, E12.4/
3 // 10X, 21HNORMAL PRESSURES (PN)00001640
4 // 53X, 2HPN // (148, E12.4) )
C
40 CALL DEFLTIN
C
50 CALL PATH
IF( SL1 ) 5,60,25
C
60 CALL INTLDS
C
FOURIER SUMMING
70 CALL SUMS
IF( SL1 ) 5,25,72
C
72 IF(ENFL - ENF .GT. 1.E-2) GO TO 10
IF(PIXI .EQ. 0.) GO TO 90
C
80 CALL PIX
GO TO 5
C
C ** SL1 = -1. WHEN HYDRO-DYNAMICS WAS ENTERED BEFORE PRINT. RETURN TO
STATEMENT 25. WHEN SL1 = -2., TEST WHETHER 3RD INTERVAL IS
COMPLETE. *YES, GO TO 72 *NO, GO TO 25.
C

```

```

00001490
00001500
00001510
00001520
00001530
00001540
00001550
00001560
00001570
00001580
00001590
00001600
00001610
00001620
00001630
00001640
00001650
00001660
00001670
00001680
00001690
00001700
00001710
00001720
00001730
00001740
00001750
00001760
00001770
00001780
00001790
00001800
00001810
00001820
00001830
00001840
00001850

```

```

C
C      90 IF(PNCH .EQ. 0.) GO TO 5
C
C      PUNCH 95, TIMX, ((ZP(K,L), Z2P(K,L), Z3P(K,L), K=1,3), OMG2(L)),
C      1
C      95 FORMAT( 1P5E14.7 )
C      GO TO 5
C      END
00001860
00001870
00001880
00001890
00001900
00001910
00001920
00001930
00001940

```

\$IBFTC MADD	00001950
C MATRIX ADD SUBROUTINE	00001960
C	00001970
C ARGUMENTS	00001980
C L NO. OF ROWS	00001990
C M NO. OF COLS	00002000
C A(I,J) MRA	00002010
C B(I,J) MAD	00002020
C C(I,J) MSR	00002030
C SUBROUTINE MAD(L,M,A,B,C)	00002040
DIMENSION A(4,4), B(4,4), C(4,4)	00002050
DO 30 I=1,L	00002060
DO 30 J=1,M	00002070
30 C(I,J)=A(I,J)+B(I,J)	00002080
RETURN	00002090
END	00002100

DECK NO. 8K-903

\$IBFTC MHPY			
C	MATRIX MULTIPLY SUBROUTINE	DECK NO. 8K-901	00002270
C			00002280
C			00002290
C	ARGUMENTS		00002300
C	L NO. OF ROWS X MATRIX		00002310
C	M NO. OF COLS X MATRIX		00002320
C	N NO. OF COLS Y MATRIX		00002330
C	X(I,K) MRA		00002340
C	Y(K,J) MMY		00002350
C	Z(I,J) MSR		00002360
C	SUBROUTINE MMY(L,M,N,X,Y,Z)		00002370
	DIMENSION X(4,4), Y(4,4), Z(4,4)		00002380
	DO 30 I=1,L		00002390
	DO 30 J=1,N		00002400
	Z(I,J)=0.0		00002410
	DO 30 K=1,M		00002420
	30 Z(I,J)=Z(I,J)+X(I,K)*Y(K,J)		00002430
	RETURN		00002440
	END		00002450


```

DO 1 I = 1,408
1 GDA(I) = 0.
CALL DECRO(GDA)
N = EN
NN = N - 1
ENS = EN
00003410
00003420
00003430
00003440
00003450
00003460

C
IF (GMI - 2.0) 20, 35, 50
00003480
00003490
00003500
00003510
00003520
00003530
00003540
00003550
00003560
00003570
00003580
00003590
00003600
00003610
00003620

C
CONE - CYLINDER
**
20 IF (PFLAG .NE. 0.0) WRITE(6,22) N, RAI, AXL, ANX
22 FORMAT(1H1,31X,34HGEOMETRY DATA FOR CONE OR CYLINDER// 35X,22HNUMB00003540
IER OF STATIONS - ,14//6X,7HRAI =,1PE13.4,7X,7HAXL =,E13.4,7X,00003550
2 7HANX =,E13.4)
00003560
00003570
00003580
00003590
00003600
00003610
00003620

C
DEL = AXL/LEN - 1.0)
SINFI = SIND(ANX)
COSFI = COSD(ANX)
WTH(1) = A0 * COSFI/RAI
WFE(1) = 0.0
RHOX(1) = RAI/A0
R(1) = RAI
00003630
00003640
00003650
00003660
00003670
00003680
00003690
00003700
00003710
00003720
00003730
00003740
00003750
00003760
00003770

C
DO 30 I = 2,N
R(I) = R(I-1) + DEL * SINFI
WTH(I) = A0 * COSFI /R(I)
WFE(I) = 0.0
30 RHOX(I) = R(I)/A0
GC TO 150
C
C
C
SPHERE - TOROID
**
35 IF (PFLAG .NE. 0.0) WRITE (6,37) IRGN, N, RC, ROFF, PHIO, PHIN
37 FORMAT(1H1,31X,24HGEOMETRY DATA FOR REGION, 13,18H (SPHERE - TORO100003760
XD) //
35X,22HNUMB00003770

```

```

IER OF STATIONS - ,I4//6X,7HRC      =,1PE13.4,7X,7HROFF  =,E13.4,7X,00003780
2 7HPHIO =,E13.4,7X,7HPHIN =,E13.4 )
  ANGSP = PHIN - PHIO
C
  DEL = ANGSP/(EN - 1.0)
  AM = 1.0
  AMU = SIGN(AM,DEL)
  BPHI = PHIO
  BSINP = SIND(PHIO)
  BCOSP = COSD(PHIO)
  R(I) = RC * BSINP + ROFF
C
  DO 40 I = 1,NN
  APTI = BPHI + DEL
  ASINP = SIND(APTI)
  ACOSP = COSD(APTI)
  R(I+1) = R(I) + RC * (ASINP - BSINP)
  WFE(I) = A0 / RC * AMU
  IF(ROFF .EQ. 0.0) GO TO 38
  WTH(I) = A0 * BSINP / R(I)
  GO TO 39
38 WTH(I) = WFE(I)
39 RHOX(I) = R(I)/A0
  BPHI = APTI
  BSINP = ASINP
  BCOSP = ACOSP
40 CONTINUE
  DEL = ABS(DEL)
  WFE(N) = A0/RC * AMU
  IF(ROFF .EQ. 0.0) GO TO 45
  WTH(N) = A0 * BSINP / R(N)
  GO TO 46
45 WTH(N) = WFE(N)
46 RHOX(N) = R(N)/A0
  DEL = DEL * RC * 0.01745329
  GO TO 150
C
00003790
00003800
00003810
00003820
00003830
00003840
00003850
00003860
00003870
00003880
00003890
00003900
00003910
00003920
00003930
00003940
00003950
00003960
00003970
00003980
00003990
00004000
00004010
00004020
00004030
00004050
00004060
00004070
00004080
00004090
00004100
00004110
00004120
00004130
00004140
00004150

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```

C      50 IF(GMI - 4.0) 75, 51, 51
C      51 WRITE (6,55)
C      55 FORMAT (/// 5X, 44HARBITRARY FUNCTIONS AND CONICS NOT AVAILABLE )
C      CALL EXIT
C      STOP
C      GENERAL DISCRETE POINTS
C      75 M = EM
C      MM = M - 1
C      MM2 = M - 2
C      IF (PFLAG .NE. 0.0) WRITE(6,76)IRGN,N, (RIPT(I), XIPT(I), I = 1,M)00004280
C      76 FORMAT(1H1,31X,24HGEOMETRY DATA FOR REGION, 13,18H (DISCRETE POINT00004290
C      1S) //35X,20HNUMBER OF STATIONS - ,14//16X,1HR,16X,2HXI //
C      2 (3X,1P2E20.7) )
C      SARB(1) = 0.0
C      IF (GMI) 92, 77, 77
C      77 DO 90 IL = 1,MM
C      SURB = 0.0
C      DLT = XIPT(IL+1) - XIPT(IL)
C      K = 10
C      AK = K
C      DDL = DLT/AK
C      KPI = K + 1
C      DO 80 JI = 1,KPI
C      AJI = JI - 1
C      XJ(JI) = XIPT(IL) + AJI * DDL
C      80 CONTINUE
C      CALL CODIMA (KPI,XJ, RRJ, XIPT, RIPT, M, 1.0)
C      DO 84 I = 2,K
C      84 RJ(I) = (RRJ(I-1) + RRJ(I) + RRJ(I+1) )/3.0
C      RJ(1) = RRJ(1)
C      RJ(KPI) = RRJ(KPI)
00004160
00004170
00004180
00004190
00004200
00004210
00004220
00004230
00004240
00004250
00004260
00004270
00004280
00004290
00004300
00004310
00004320
00004330
00004340
00004350
00004360
00004370
00004380
00004390
00004400
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00004430
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00004460
00004470
00004480
00004490
00004500
00004510
00004520

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```

C
DO 86 JR = 1,K
DLR(JR) = RJ(JR+1) - RJ(JR)
DLS = SORT(DLR(JR)**2 + DDL**2)
86 SURB = SURB + DLS
SARB(IL+1) = SARB(IL) + SURB
90 CONTINUE
GC TO 96
92 DO 94 I = 1,M
94 SARB(I) = XIPT(I)
96 DEL = SARB(M) / (EN - 1.0)
C
SURF(1) = 0.0
DO 98 I = 1,NN
98 SURF(I+1) = SURF(I) + DEL
CALL CODIMA(N, SURF,RCRV, SARB, RCURV, M, 1.0)
CALL CODIMA(N,SURF, PCRZ, SARB, RCURZ, M, 1.0)
C
100 CALL CODIMA (N,SURF, R, SARB, RIPT, M, 1.0)
105 MLN = N - 2
NSM = 1
110 DO 115 I = 3,MLN
RR(I) = (-3.*R(I-2) + 12.*R(I-1) + 17.*R(I) + 12.*R(I+1)) - 3. *
1 R(I+2) )/ 35.0
115 CONTINUE
RR(NN) = R(NN)
RR(2) = R(2)
RR(N) = R(N)
RR(1) = R(1)
IF (NSM.EQ. 25) GO TO 125
NSM = NSM + 1
DO 120 I = 1,N
120 R(I) = RR(I)
GO TO 110
125 RHOX(1) = RR(1)/AO
DELSQ = DEL * DEL
DO 130 I = 1,NN
00004530
00004540
00004550
00004560
00004570
00004580
00004590
00004600
00004610
00004620
00004630
00004640
00004650
00004660
00004670
00004680
00004690
00004700
00004710
00004720
00004730
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00004750
00004760
00004770
00004780
00004790
00004800
00004810
00004820
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00004880
00004890

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```

GO TO 210
208 GAMA(I) = 0.0
210 CONTINUE
C
220 IF (PFLAG.EQ. 0.0) GO TO 1000
C
WRITE (6,230) (I, R(I), WTH(I), WFE(I), RHOX(I), GAMA(I),
1 I = 1,N)
230 FORMAT (1H-,9X,1H,9X,4HR(I), 10X,8HW(THETA),11X,
1 5HW(X1),11X,7HRHOX(I),10X,7HGAMA(I) //(11,1P5E17.7) )
C
1000 DEL2 = 2. * DEL
BTAL1 = -S77 * CFE * DEL
BTA33 = -S77 * CZ * DEL
C
EN1 = 1.
1005 IF(R(I).NE. 0.) GO TO 2000
C
EN1 = 2.
DO 1010 I = 1,4
EM6(I) = 0.
DC 1010 J = 1,4
EM2(I,J) = 0.
1010 EM4(I,J) = 0.
C FORM UPPER BOUNDARY MATRICES FOR CLOSED SHELL
EM4(1,1) = 1.
IF(ENF - 1.) 1120,1130,1140
1120 EM2(4,4) = 1. /DEL
1121 EM2(3,3) = 1. /DEL
EM4(2,2) = 1.
GC TO 2000
1130 EM2(2,1) = 1. /DEL
EM4(1,2) = 1.
1135 EM4(3,3) = 1.
EM4(4,4) = 1.
GC TO 2000
1140 IF(ENF.NE. 2.) GO TO 1150

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00005270
00005280
00005290
00005300
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00005320
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00005370
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00005400
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00005500
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00005570
00005580
00005590
00005600
00005610
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00005630

```

EM4(4,3) = 1.
 GC TO 1121
 1150 EM4(2,2) = 1.
 GO TO 1135

C

2000 RETURN
 END

00005640
 00005650
 00005660
 00005670
 00005680
 00005690
 00005700

```

$IBFTC CF3P
C PARABOLIC CURVE FITTING SUBROUTINE (THREE POINTS)
C
C SUBROUTINE CODIMA (N1, X, Y, XI, YI, N2, SHAPE)
C
C ARGUMENTS
C N1 NO. OF POINTS TO INTERPOLATE
C X LOCATION OF POINTS TO BE INTERPOLATED
C Y ANSWERS
C XI INDEPENDENT ARGUMENT
C YI DEPENDENT ARGUMENT
C N2 NO. OF ARGUMENTS
C SHAPE 0 = FITS END WITH STRAIGHT LINE 1 = CURVE, LAST 3 PTS.
C
C DIMENSION X(1),Y(1),XI(1),YI(1),D(2),A(2),B(2),C(2)
C
C 100 IN = 0
C XK = SHAPE
C
C DO 800 N = 1,N1
C
C IF (N2-2) 110,115,120
C 110 Y(N) = YI(N2)
C GO TO 800
C
C 115 Y(N) = (YI(2)-YI(1))/(XI(2)-XI(1))* (X(N)-XI(1))+YI(1)
C GO TO 800
C
C 120 J = 1
C 125 IF(XI(J)-X(N)) 130,140,150
C 140 Y(N) = YI(J)
C GO TO 800
C
C 130 J = J+1
C IF(J-N2) 125,125,145
C 145 Y(N) = (YI(N2)-YI(N2-1))/(XI(N2)-XI(N2-1))*(X(N)-XI(N2-1))
C 1 + YI(N2 - 1)

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00005980
00005990
00006000
00006010
00006020
00006030
00006040
00006050
00006060
00006070

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```

C
GO TO 800
150 IF(J-2) 115,155,160
155 K = 3
JJ = 1
GO TO 185
160 IF(J-N2) 170,165,145
165 K = N2-1
JJ = 2
GO TO 185
170 IF(J-IN) 180,300,180
180 JJ = 3
K = J
C
185 DO 200 M = 1,2
X1 = XI(K-1)-XI(K)
X2 = XI(K)-XI(K-2)
X3 = XI(K-2)-XI(K-1)
Y1 = YI(K-1)-YI(K)
Y2 = YI(K)-YI(K-2)
Y3 = YI(K-2)-YI(K-1)
XX1 = XI(K-2)**2
XX2 = XI(K-1)**2
XX3 = XI(K)**2
D(M) = XX1*X1 + XX2*X2 + XX3*X3
A(M) = (YI(K-2)*X1 + YI(K-1)*X2 + YI(K)*X3)/D(M)
B(M) = (XX1*Y1 + XX2*Y2 + XX3*Y3)/D(M)
C(M) = YI(K-2) - A(M)*XX1 - B(M)*XI(K-2)
200 K = K+1
300 P1 = X(N)*(A(1)*X(N)+B(1)) + C(1)
P2 = X(N)*(A(2)*X(N)+B(2)) + C(2)
AL = (X(N)-XI(J-1))/(XI(J)-XI(J-1))
S = YI(J)*AL + YI(J-1)*(1.0-AL)
GO TO (320,330,350),JJ
C
320 P2 = P1
AL = (X(N)-XI(1))/(XI(2)-XI(1))

```

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00006080
00006090
00006100
00006120
00006130
00006140
00006150
00006160
00006170
00006180
00006190
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00006220
00006230
00006240
00006250
00006260
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00006290
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00006340
00006350
00006360
00006370
00006380
00006390
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00006450

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```

      S = AL*YI(2) + (1.0-AL)*YI(1)
      IF (SHAPE) 321,322, 322
321  XM1 = ABS (YI(2) - YI(1)) / (XI(2) - XI(1))
      XM2 = ABS (YI(3) - YI(2)) / (XI(3) - XI(2))
      XK = 1. - ABS (XM1 -XM2) / (XM1 + XM2)
322  P1 = S + XK *(P2-S)
      GO TO 350
C
330  P1 = P2
      AL = (X(N)-XI(N2-1)) / (XI(N2)-XI(N2-1))
      S = AL* YI(N2) +(1.0-AL)*YI(N2-1)
      IF (SHAPE) 331,332, 332
331  XM1 = ABS (YI(N2 - 1) - YI(N2)) / (XI(N2 -1) - XI(N2))
      XM2 = ABS (YI(N2 -2) - YI(N2 -1)) / (XI(N2 -2) - XI(N2 -1))
      XK = 1. - ABS (XM1 -XM2) / (XM1 + XM2)
332  P2 = S + XK*(P1-S)
C
350  E1 = ABS (P1-S)
      E2 = ABS (P2-S)
      IN = J
      IF(E1+E2) 700,700,750
700  Y(N) = S
      GO TO 800
750  YNUM = E1 * AL * P2 + (1. - AL) * E2 * P1
      YDEN = E1 * AL + (1. - AL) * E2
      Y(N) = YNUM / YDEN
800  CCNTINUE
C
900  RETURN
      END

```

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00006460
00006470
00006480
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00006500
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00006570
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00006590
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00006620
00006630
00006640
00006650
00006660
00006670
00006680
00006690
00006700
00006710
00006720
00006730
00006740
00006750

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$1BFTC CDAFIT
C CURVE FIT SUBROUTINE 6J-157DR
C SUBROUTINE CRVFIT
C
C THE NOMENCLATURE IS VERY SIMILAR TO THAT IN THE DA DATA REGION
C AS EXPLAINED IN THE EXECUTIVE PROGRAM. THE SUFFIX TB (TABLE)
C HAS BEEN ADDED TO EACH PARAMETER.
C
C THE TABLES ARE SET UP AS FOLLOWS
C TAB(1) NO. OF STATIONS GIVEN
C TAB(2) STATION NO. = 1.
C TAB(3) PARAMETER VALUE AT STATION 1.
C TAB(4)FF STATIONS AND VALUES INTERLACED.
C THE LAST STATION MUST BE N BECAUSE CODIMA WILL NOT EXTRAPOLATE
C
C REAL MASS, MO
C
C DIMENSION CDA(697), DTB(41), EKT(41), EITB(41), ALFTB(41),
1 DNATB(41), TT(41), ENTB(41), ENT(41), PNTB(41), PFETB(41),
2 PTHTB(41), DZOTB(41), VZOTB(41), QZOTB(41), DFOTB(41),
3 VFOTB(41), QFOTB(41),
4 D(200), EK(200), EI(200), ALF(200), DNA(200), T(200), ENT(200),
5 EMT(200), PNI(200), PFE(200), PTH(200), DZO(200), VZO(200),
6 AZO(200), DFO(200), VFO(200), AFO(200), X(200),
7 STA(20), VAL(20)
C
C EQUIVALENCE
1(CDA(83), EITB), (CDA(1), DTB), (CDA(42), EKT),
2(CDA(206), TT), (CDA(124), ALFTB), (CDA(165), DNATB),
3(CDA(329), PNTB), (CDA(247), ENT), (CDA(288), EMT),
4(CDA(452), DZOTB), (CDA(370), PFETB), (CDA(411), PTHTB),
5(CDA(575), DFOTB), (CDA(493), VZOTB), (CDA(534), QZOTB),
(CDA(616), VFOTB), (CDA(657), QFOTB)
C
C EQUIVALENCE (DA(1), EN ),(DA(25), MASS ),(DA(1040), D ),(DA(1240),
1(DA(1240), EK ),(DA(1440), E1 ),(DA(1640), ALF ),(DA(1840), DNA),00007130
2(DA(2040), T ),(DA(2240), ENT), (DA(2440), EMT ),(DA(2640), PN ),00007140

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3(DA(2840), PFE ),(DA(3040), PTH),(DA(3240), DZO ),(DA(3440), VZO),00007150
4(DA(3640), AZO ),(DA(3840), DFO),(DA(4040), VFO ),(DA(4240), AFO),00007160
5(DA(3), HO ),(DA(4), EO ),(DA(8), POI ),(DA(16), ENFO ),00007170
6(DA(36), RESTRT)
00007180
00007190
C
COMMON DA(4511), EM2(4,4), EM4(4,4), EM6(4,4), S1, S2, ELAM2,
1 Z(4,200),XX(4,200), A2(4,4), B2(4,4), C2(4,4), G2(4,4), E(4,4),
2 F(4,4), GA(4,4), A(4,4), B(4,4), C(4,4), G(4,4), EC(4,4), DEL2,
3 SL1, SL2, N, NTH, NTPR, NTPM, I, K, L,
4 S77, S78, BTA11, BTA33, MO(200), OMG2(200), ZP(3,200),
5 Z2P(3,200), Z3P(3,200), TIMX, TDEL, PRNT, ENF, PRI, JT
00007250
00007260
00007270
00007280
00007290
00007300
00007310
C
CALL DECRO ( COA )
00007320
C
IF(RESTRT .EQ. 0.) GO TO 65
00007330
00007340
00007350
C
READ ( 5,55) TIMX, ((ZP(K,L), Z2P(K,L), Z3P(K,L), K=1,3),
1 OMG2(L), L=1,N)
00007370
55 FORMAT( 1P5E14.7 )
00007380
TIMX = TIMX + TDEL
00007390
JT = TIMX /TDEL + 0.01
00007400
PRNT = JT
00007410
C
PRINT TABLES ON NEG. IND.
00007420
00007430
00007440
C
WRITE ( 6,70) (I, DTB(I), EKTB(I), ELTB(I), ALFTB(I), DNATB(I),
1 ITB(I), ENTB(I), EMTB(I), I = 1,41)
00007450
70 FORMAT(///10X, 16HCURVE FIT TABLES ///14X,3HDTB, 8X,4HEKTB, 8X,
1 4HELTB, 8X,5HALFTB, 7X,5HDNATB, 8X,3HTTB, 8X,4HEMTB, 8X,4HEMTB //00007480
2 (18, 1P8E12.3) )
00007490
00007500
C
WRITE ( 6,72) (I, PNTB(I), PFETB(I), PHTB(I), DZOTB(I),
00007510

```

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1  VZOTB(I), QZOTB(I), DFOTB(I), VFOTB(I), QFOTB(I), I = 1,41)
72 FORMAT(/// 11X,4HPNTB, 6X,5HPFEIB, 6X,5HPHTIB, 6X,5HDZOTB, 6X,
1  5HVZOTB, 6X,5HQZOTB, 6X,5HVFOTB, 6X,5HVFOTB, 6X,5HQFOTB //
2  (16, IP9E11.2) )
C
90 DO 92 I = 1,N
92 X(I) = I
C
100 IF(DTB.NE. 1.E+10) GO TO 120
DO 105 I = 1,N
105 D(I) = DTB(2)
GO TO 200
C
120 IF(DTB.EQ. 0.) GO TO 600
NOSTA = DTB
ICDA = 1
ICA = 1040
IXX = 1
GO TO 2000
C
200 IF(EKTB.NE. 1.E+10) GO TO 220
DO 205 I = 1,N
205 EK(I) = EKTB(2)
GO TO 300
C
220 NOSTA = EKTB
ICDA = 42
ICA = 1240
IXX = 2
GO TO 2000
C
300 IF(EITB.NE. 1.E+10) GO TO 320
DO 305 I = 1,N
305 EI(I) = EITB(2)
GO TO 400
C
320 NOSTA = EITB

```

FORM COL. OF STATION NOS.

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00007520
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00007690
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00007800
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C
  ICDA = 83
  IDA = 1440
  IXX = 3
  GO TO 2000

  400 IF(ALFTB .NE. 1.E+10) GO TO 420
  DO 405 I = 1,N
  405 ALF(I) = ALFTB(2)
  GO TO 500

C
  420 IF(ALFTB .EQ. 0.) GO TO 500
  NOSTA = ALFTB
  ICDA = 124
  IDA = 1640
  IXX = 4
  GO TO 2000

C
  500 IF(DNATB .NE. 1.E+10) GO TO 520
  DO 505 I = 1,N
  505 DNA(I) = DNATB(2)
  505 MO(I) = MASS * D(I) / EI(I) * S3
  GO TO 600

C
  520 NOSTA = DNATB
  ICDA = 165
  IDA = 1840
  IXX = 5
  GO TO 2000

C
  580 DO 582 I = 1,N
  582 MC(I) = MASS * D(I) / EI(I) * S3

C
  600 IF(TTB .NE. 1.E+10) GO TO 620
  DO 605 I = 1,N
  605 T(I) = TTB(2)
  GO TO 700

C

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00007900
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00007970
00007980
00007990
00008000
00008010
00008020
00008030
00008040
00008050
00008060
00008070
00008080
00008090
00008100
00008110
00008120
00008130
00008140
00008150
00008160
00008170
00008180
00008190
00008200
00008210
00008220
00008230
00008240
00008250

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620 IF( TT8 )      622,900,630
622 NOSTA = -TT8
   ICDA = 206
   IDA = 2040
   IXX = 6
   GO TO 2000
C
630 DO 632      I = 1,N
632 T(I) = ENTERP( X(I), TT8)
C
700 IF(ENTB .NE. 1.E+10) GO TO 720
   DO 705      I = 1,N
705 ENT(I) = ENTB(2)
   GO TO 800
C
720 IF( ENTB )      722,800,730
722 NOSTA = -ENTB
   ICDA = 247
   IDA = 2240
   IXX = 7
   GO TO 2000
C
730 DO 732      I = 1,N
732 ENT(I) = ENTERP( X(I), ENTB)
C
800 IF(EMTB .NE. 1.E+10) GO TO 820
   DO 805      I = 1,N
805 EMT(I) = EMTB(2)
   GO TO 900
C
820 IF( EMTB )      822,900,830
822 NOSTA = -EMTB
   ICDA = 288
   IDA = 2440
   IXX = 8
   GO TO 2000
C

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00008260
00008270
00008280
00008290
00008300
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00008390
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00008600
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00008620

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830 DO 832 I = 1,N
832 EMT(I) = ENTERP( X(I), EMTB)
C
900 IF(PNTB.NE. 1.E+10) GO TO 920
DO 905 I = 1,N
905 PN(I) = PNTB(2)
GO TO 1000
C
920 IF( PNTB ) 922,1000,930
922 NOSTA = -PNTB
ICDA = 329
ICA = 2640
IXX = 9
GO TO 2000
C
930 DO 932 I = 1,N
932 PN(I) = ENTERP( X(I), PNTB)
C
1000 IF(PFETB.NE. 1.E+10) GO TO 1020
DO 1005 I = 1,N
1005 PFE(I) = PFETB(2)
GO TO 1100
C
1020 IF( PFETB ) 1022,1100,1030
1022 NOSTA = -PFETB
ICDA = 370
ICA = 2840
IXX = 10
GO TO 2000
C
1030 DO 1032 I = 1,N
1032 PFE(I) = ENTERP( X(I), PFETB)
C
1100 IF(PHTB.NE. 1.E+10) GO TO 1120
DO 1105 I = 1,N
1105 PTH(I) = PHTB(2)
GO TO 1200

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00008980
00008990

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C	1120 IF(PTHB)	1122,1200,1130	00009000
	1122 NOSTA = -PTHB		00009010
	ICDA = 411		00009020
	ICA = 3040		00009030
	IXX = 11		00009040
	GO TO 2000		00009050
C			00009060
	1130 DO 1132 I = 1,N		00009070
	1132 PTH(I) = INTERP(X(I), PTHB)		00009080
C			00009090
	1200 IF(DZOTB.NE. 1.E+10) GO TO 1220		00009100
	DO 1205 I = 1,N		00009110
	1205 DZO(I) = DZOTB(2)		00009120
	GO TO 1300		00009130
C			00009140
	1220 IF(DZOTB)	1222,2100,1230	00009150
	1222 NOSTA = -DZOTB		00009160
	ICDA = 452		00009170
	IDA = 3240		00009180
	IXX = 12		00009190
	GO TO 2000		00009200
C			00009210
	1230 DO 1232 I = 1,N		00009220
	1232 DZO(I) = INTERP(X(I), DZOTB)		00009230
C			00009240
	1300 IF(VZOTB.NE. 1.E+10) GO TO 1320		00009250
	DO 1305 I = 1,N		00009260
	1305 VZO(I) = VZOTB(2)		00009270
	GO TO 1400		00009280
C			00009290
	1320 IF(VZOTB)	1322,1400,1330	00009300
	1322 NOSTA = -VZOTB		00009310
	ICDA = 493		00009320
	IDA = 3440		00009330
	IXX = 13		00009340
	GO TO 2000		00009350
			00009360

```

C      1330 DO 1332 I = 1,N
      1332 VZ0(I) = ENTERP( X(I), VZ0TB)
C
      1400 IF(QZ0TB.NE. 1.E+10) GO TO 1420
      DO 1405 I = 1,N
      1405 AZ0(I) = QZ0TB(2) /M0(I)
      GO TO 1500
C
      1420 IF( QZ0TB ) 1422,1500,1430
      1422 NOSTA = -QZ0TB
      ICDA = 534
      IDA = 3640
      IXX = 14
      GO TO 2000
C
      1430 DO 1432 I = 1,N
      QZ0 = ENTERP( X(I), QZ0TB)
      1432 AZ0(I) = QZ0 /M0(I)
      GO TO 1500
C
      1480 DO 1482 I = 1,N
      1482 AZ0(I) = AZ0(I) /M0(I)
C
      1500 IF(DF0TB.NE. 1.E+10) GO TO 1520
      DO 1505 I = 1,N
      1505 DF0(I) = DF0TB(2)
      GO TO 1600
C
      1520 IF( DF0TB ) 1522,1600,1530
      1522 NOSTA = -DF0TB
      ICDA = 575
      IDA = 3840
      IXX = 15
      GO TO 2000
C
      1530 DO 1532 I = 1,N

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00009390
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00009690
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00009710
00009720
00009730

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1532	DF0(I) =	INTERP(X(I), DF0TB)	00009740
C			00009750
1600	IF(VF0TB .NE. 1.E+10)	GO TO 1620	00009760
	DO 1605	I = 1,N	00009770
1605	VF0(I) =	VF0TB(2)	00009780
	GO TO	1700	00009790
C			00009800
1620	IF(VF0TB)	1622,1700,1630	00009810
1622	NOSTA =	-VF0TB	00009820
	ICDA =	616	00009830
	IDA =	4040	00009840
	IXX =	16	00009850
	GC TO	2000	00009860
C			00009870
1630	DO 1632	I = 1,N	00009880
1632	VF0(I) =	INTERP(X(I), VF0TB)	00009890
C			00009900
1700	IF(QF0TB .NE. 1.E+10)	GO TO 1720	00009910
	DO 1705	I = 1,N	00009920
1705	AF0(I) =	QF0TB(2) /MO(I)	00009930
	GO TO	2100	00009940
C			00009950
1720	IF(QF0TB)	1722,2100,1730	00009960
1722	NOSTA =	-QF0TB	00009970
	ICDA =	657	00009980
	IDA =	4240	00009990
	IXX =	17	00010000
	GC TO	2000	00010010
C			00010020
1730	DO 1732	I = 1,N	00010030
	QF0 =	INTERP(X(I), QF0TB)	00010040
1732	AF0(I) =	QF0 /MO(I)	00010050
	GO TO	2100	00010060
C			00010070
1780	DO 1782	I = 1,N	00010080
1782	AF0(I) =	AF0(I) /MO(I)	00010090
	GC TO	2100	00010100

```

C      2000 K0 = 0
      K2 = 2 * NOSTA
      DO 2005 I = 2,K2,2
      K0 = K0 + I
      KX = ICDA + I - 1
      STA(K0) = CDA(KX)
      2005 VAL(K0) = CDA(KX+1)
      CALL CODIM4 (N,X,DA(IDA), STA,VAL,NOSTA, 1.)
C
      GO TO (200, 300, 400, 500, 580, 700, 800, 900, 1000, 1100, 1200,
      1 1300, 1400, 1480, 1600, 1700, 1780), IXX
C
      2100 IF(TIMX.NE.TDEL) GO TO 3050
      IF(ENF.NE.ENFO) GO TO 5000
      TDEL2 = TDEL **2
      DO 2110 I = 1,N
      OMG2(I) = S77 * M0(I) * S78
      ZP(1,I) = DF0(I)
      ZP(3,I) = DZ0(I)
      Z2P(1,I) = AF0(I) * TDEL2 + 2. * DF0(I)
      Z2P(3,I) = AZ0(I) * TDEL2 + 2. * DZ0(I)
      Z3P(1,I) = 6. * (AF0(I)*TDEL2 + VF0(I)*TDEL) + 9. * DF0(I)
      Z3P(3,I) = 6. * (AZ0(I)*TDEL2 + VZ0(I)*TDEL) + 9. * DZ0(I)
      2110 Z3P(3,I) =
C
      WRITE (6,3000) (DA(I), I=1,32), DA(4441), DA(4477), (I, D(I),
      1 EK(I), EI(I), ALF(I), DNA(I), T(I), ENT(I), EMT(I), I = 1,N)
      3000 FORMAT( 1H1//10X, 12HINITIAL DATA// 6X,7HEN =,1PE12.3, 8X,
      1 7HA0 =,E12.3, 8X,7HH0 =,E12.3, 8X,7HE0 =,E12.3// 6X,
      2 7HSIG0 =,E12.3, 8X,7HENF0 =,E12.3, 8X,7HENFL =,E12.3, 8X,
      3 7HPOI =,E12.3// 6X,7HTHETA =,E12.3, 8X,7HPXI =,E12.3, 8X,
      4 7HSPRL =,E12.3, 8X,7HUK =,E12.3// 6X,7HVK =,E12.3, 8X,
      5 7HWK =,E12.3, 8X,7HEMK =,E12.3, 8X,7HTAU1 =,E12.3 // 6X,
      6 7HENT1 =,E12.3, 8X,7HP11 =,E12.3, 8X,7HTAU2 =,E12.3, 8X,
      7 7HENT2 =,E12.3// 6X,7HP12 =,E12.3, 8X,7HTAU3 =,E12.3, 8X,
      8 7HENT3 =,E12.3, 8X,7HP13 =,E12.3// 6X,7HMASS =,E12.3, 8X,
      9 7HCFE =,E12.3, 8X,7HCKZ =,E12.3, 8X,7HCKFE =,E12.3// 6X,

```

```

X 7HSKZ      =,E12.3, 8X,7HSUM      =,E12.3, 8X,7HEN1      =,E12.3, 8X,      00010480
1 7HDEL      =,E12.3// 6X,7HBCITP =,E12.3, 8X,7HBC18M =,E12.3// 15X,      00010490
2 1HD, 10X,2HEK, 10X,2HE1, 10X,3HALF, 9X,3HDNA, 10X,1HT, 10X,      00010500
3 3HENT, 9X,3HEMT // (18, 8E12.3) )      00010510
WRITE (6,3005) (I, PN(I), PFE(I), PTH(I), OZO(I), VZO(I),      00010520
1 AZO(I), DFO(I), VFO(I), AFO(I), I = 1,N)      00010530
3005 FORMAT(/// 12X,2HPN, 8X,3HPFE, 8X,3HPTH, 8X,3HDZO, 8X,3HVZO, 8X,      00010540
1 3HAZO, 8X,3HDOFO, 8X,3HVFO, 8X,3HAFO // (16, 1P9E11.2) )      00010550
C                                          00010560
GO TO 5000                                00010570
3050 WRITE(6,3052)TIMX,(I, T(I), ENT(I), EMT(I), PFE(I), PTH(I), PN(I),      00010580
1 I = 1,N)                                00010590
3052 FORMAT(///10X, 9HAT TIME =,1PE10.3,15H THE LOADS WERE // 5X,1HI,      00010600
1 11X,1HT, 14X,3HENT, 13X,3HEMT, 13X,3HPFE, 13X,3HPTH, 14X,2HPN//      00010610
2 (16,6E16.3) )                          00010620
C                                          00010630
5000 RETURN                                00010640
END                                          00010650

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```

C      GO TO 800
      150 IF(J-2) 115,155,160
      155 K = 3
      JJ = 1
      GO TO 185
      160 IF(J-N2) 170,165,145
      165 K = N2-1
      JJ = 2
      GO TO 185
      170 IF(J-IN) 180,300,180
      180 JJ = 3
      K = J
C
      185 DO 200 M = 1,2
      X1 = XI(K-1)-XI(K)
      X2 = XI(K)-XI(K-2)
      X3 = XI(K-2)-XI(K-1)
      Y1 = YI(K-1)-YI(K)
      Y2 = YI(K)-YI(K-2)
      Y3 = YI(K-2)-YI(K-1)
      XX1 = XI(K-2)**2
      XX2 = XI(K-1)**2
      XX3 = XI(K)**2
      D(M) = XX1*X1 + XX2*X2 + XX3*X3
      A(M) = (YI(K-2)*X1 + YI(K-1)*X2 + YI(K)*X3)/D(M)
      B(M) = (XX1*Y1 + XX2*Y2 + XX3*Y3)/D(M)
      C(M) = YI(K-2) - A(M)*XX1 - B(M)*XI(K-2)
      200 K = K+1
      300 P1 = X(N)*(A(1)*X(N)+B(1)) +C(1)
      P2 = X(N)*(A(2)*X(N)+B(2)) +C(2)
      AL = (X(N)-XI(J-1))/(XI(J)-XI(J-1))
      S = YI(J)*AL + YI(J-1)*(1.0-AL)
      GO TO (320,330,350),JJ
C
      320 P2 = P1
      AL = (X(N)-XI(1))/(XI(2)-XI(1))

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00011180
00011190
00011200
00011210
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00011380
00011390
00011400

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S = AL*YI(2) + (1.0-AL)*YI(1)	00011410
IF (SHAPE) 321,322, 322	00011420
321 XM1 = ABS (YI(2) - YI(1)) / (XI(2) - XI(1))	00011430
XM2 = ABS (YI(3) - YI(2)) / (XI(3) - XI(2))	00011440
XK = 1. - ABS (XM1 - XM2) / (XM1 + XM2)	00011450
322 P1 = S + XK *(P2-S)	00011460
GO TO 350	00011470
C	00011480
330 P1 = P2	00011490
AL = (X(N)-XI(N2-1)) / (XI(N2)-XI(N2-1))	00011500
S = AL* YI(N2) + (1.0-AL)*YI(N2-1)	00011510
IF (SHAPE) 331,332, 332	00011520
331 XM1 = ABS (YI(N2 - 1) - YI(N2)) / (XI(N2 - 1) - XI(N2))	00011530
XM2 = ABS (YI(N2 - 2) - YI(N2 - 1)) / (XI(N2 - 2) - XI(N2 - 1))	00011540
XK = 1. - ABS (XM1 - XM2) / (XM1 + XM2)	00011550
332 P2 = S + XK*(P1-S)	00011560
C	00011570
350 E1 = ABS (P1-S)	00011580
E2 = ABS (P2-S)	00011590
IN = J	00011600
IF(E1+E2) 700,700,750	00011610
700 Y(N) = S	00011620
GO TO 800	00011630
750 YNUM = E1 * AL * P2 + (1. - AL) * E2 * P1	00011640
YDEN = E1 * AL + (1. - AL) * E2	00011650
Y(N) = YNUM / YDEN	00011660
800 CONTINUE	00011670
C	00011680
900 RETURN	00011690
END	00011700


```

$IBFTC ENTP
C      LINEAR INTERPOLATION SUBROUTINE **ENTERP**
C
C      SELECTS THE VALUE AT EITHER END OF TABLE WHEN ARGUMENT EXCEEDS
C      LIMIT, THEN CONTINUES
C
C      SUBROUTINE ARGUMENTS
C      X      VALUE TO LOOK UP IN TABLE
C      TAB(1) NO. OF PAIRS OF ARGUMENTS AND VALUES IN TABLE
C      TAB(2), ETC ARGUMENTS AND FUNCTIONS INTERLACED
C
C      FUNCTION ENTERP (X, TAB)
C
C      DIMENSION TAB(101)
C      IF (TAB) 9,9,8
C      9 ENTERP = - TAB
C      RETURN
C
C      8 N = TAB
C      DO 5 I=1,N
C      1 IF (TAB(2*I)-X) 5,4,3
C      3 IF (I-1) 6,6,7
C      7 ENTERP = TAB(2*I-1) + (X-TAB(2*I-1)) * (TAB(2*I+1) - TAB(2*I-1))
C      5 / (TAB(2*I) - TAB(2*I-2))
C      RETURN
C      4 ENTERP = TAB(2*I+1)
C      RETURN
C      5 CONTINUE
C      M = 2*N+1
C      K = M
C
C      105 WRITE ( 6,10) X, TAB(K)
C      10 FORMAT (// 10X, 39HLIMITS OF TABLE EXCEEDED BY ARGUMENT = 1PE12.4
C      1 / 10X, E12.4, 24H = VALUE USED FROM TABLE )
C      ENTERP = TAB(K)
C      RETURN
C      6 M = 2*N+1
C      K = 3
C      GO TO 105
C      END

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$IBFTC ACCN1
C CALCULATION OF HYDRO PRESSURE PROFILES BY USING LAMBS SOLUTIONS
C
C SUBROUTINE ACCN (PMAX, RMAX)
C
C DIMENSION PM(200), RHOX(200)
C EQUIVALENCE (DA(32), DEL ),(DA(34), VIN ),(DA(35), RHO ),(DA(440), WFE ),(DA(2640), PM ),(DA(840), RHOX)
C
C COMMON DA(8520), T, IDEL, PRNT(5), WT
C
C DEL=ARC INCREMENT
C
C R=OUTER RADIUS OF SPHERE =1/WFE
C R=1.0/WFE
C
C RMAX = SQRT(2. * T * R * VIN)
C ALPHA = 4.0 /3.0
C BAF = 1.0 + ALPHA * RHO * RMAX **3 /WT
C A1 = 2. * R * VIN **2 * RHO /(3.1415927 * RMAX * 32.2 * 12.0
C
C A3 = ALPHA * RHO * RMAX **3 /WT
C N = RMAX /DEL
C NP=N+1
C
C DO 10 I=1,NP
C ROC = FLOAT(I-1) * DEL /RMAX
C PM(I) = A1 *(1. - A3*(2. - 3.*ROC **2)) / SQRT(1. - ROC **2)
C
C 10 CONTINUE
C
C A = 2. * RHO * RMAX **3 /WT
C B = A1 * RMAX * (1.0 - 4.0 * A /3.0)
C X = (FLOAT(N) + 0.5) * DEL
C
C IF(RMAX .GT. X) GO TO 20
C
C CASE I (X .GE. RMAX .GT. N*DEL)

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	PM(NP) = B *(PMAXL(RMAX, RMAX, A) - P*MAXL(X-DEL, RMAX, A))	00012470
1	/DEL		00012480
	GO TO 30		00012490
			00012500
C	CASE II (RMAX -GT. X)	00012510
	20 PM(NP+1) = B *(PMAXL(RMAX, RMAX, A) - P*MAXL(X, RMAX, A))	00012520
1	/DEL		00012530
			00012540
C	30 RETURN		00012550
	END		00012560

\$IBFTC PMAXX	00012570
C	00012580
FUNCTION PMAXL(R, RMAX, A)	00012590
C	00012600
RORM = R / RMAX	00012610
PMAXL = (1. + A) * ARSIN(RORM) - A * RORM * SQRT(1. - RORM **2)	00012620
C	00012630
RETURN	00012640
END	00012650

C	\$I8FTC 157DRI 6J-157DR
C	SUBROUTINE DEFLT N COMPUTES DEFLECTIONS
C	DIMENSION R(200), D(200), EK(200), ENT(200), EMT(200), PFE(200), WTHD(200)
C	1 PTH(200), PN(200), WFE(200), ALF(200), DNA(200), WTND(200),
C	2 RHDX(200), GAMA(200), EI(200), T(200), P(4,4,200), EM1(4,4,
C	3 EM3(4,4), EM5(4), EMIN(4,4), EM3N(4,4), EM5N(4)
C	REAL MASS, LM11,LM22,LM33, MM11,MN22,NM33, NM11,NM22,NM33,
C	I MO
C	EQUIVALENCE (DA(1)), EN),(DA(2)), AO),(DA(3)), HO),(DA(4)) 1(DA(4)), EO),(DA(5)), SIGO),(DA(6)), ENFO),(DA(7)), ENFL),(DA(8)), POI),(DA(9)), THETA),(DA(10)), PIXI),(DA(11)), SPRL),(DA(12)), UK),(DA(13)), VK),(DA(14)), WK),(DA(15)), EMK),(DA(16)), TAUI),(DA(17)), ENTI),(DA(18)), PIL),(DA(19)), TAUZ),(DA(20)), ENT2),(DA(21)), PI2),(DA(22)), TAU3),(DA(23)), ENT3),(DA(24)), PI3),(DA(25)), MASS),(DA(26)), CFE),(DA(27)), CZ),(DA(28)), SKFE),(DA(29)), SKZ),(DA(30)), SUM),(DA(31)), ENI),(DA(32)), DEL),(DA(36)), RESTRT)
C	RHOX(200), GAMMA(200), A(4,4), B(4,4), C(4,4), G(4), EC(4), DEL2, COMMON DA(4511), EM2(4,4), EM4(4,4), EM6(4), S1, S2, ELAM2, 1 Z(4,200), X(4,200), A2(4,4), B2(4,4), C2(4,4), G2(4), E(4,4), 2 F(4,4), GA(4,4), A(4,4), B(4,4), C(4,4), G(4), EC(4), DEL2, 3 SL1, SL2, N, NTH, NIPTW, I, K, L, 4 S7T, S7R, BTAIL, BTAT33, MC(200), DMG2(200), ZP(3,200), 5 Z2P(3,200), Z3P(3,200), TIME, IDEL, PRNT, ENF, PRI, JT, NJT, VI

```

C
C
N2 = SPRL
DO 300 I = 1,N
  WTH = WTHD(I)
  GAM = GAMA(I)
  RHO = RHOX(I)
  S4 = ELAM2 * EK(I) * S1
  S6 = 3. * WFE(I) - WTH
  S7 = 3. * WTH - WFE(I)
  S80 = -4. * OMG2(I)
  S79 = -5. * OMG2(I)
  LM11 = S79 + 6. * BTA11
  LM22 = S79
  LM33 = S79 + 6. * BTA33
  MM11 = -(S80 + 3. * BTA11)
  MM22 = -S80
  MM33 = -(S80 + 3. * BTA33)
  NM11 = -OMG2(I) + .66666667 * BTA11
  NM22 = -OMG2(I)
  NM33 = -OMG2(I) + .66666667 * BTA33
  IF(I - 1) 100, 2, 100
  2 IF(EN1 -GE. 2.) GO TO 95
C
  I = 1, OPEN APEX
  BP = (-D(3) + 4.*D(2) - 3.*D(1) /DEL2
  WFEP = (-WFE(3) + 4.*WFE(2) - 3.* WFE) /DEL2
  TTP = (-ENT(3) + 4.*ENT(2) - 3.*ENT) /DEL2
  DP = (-EK(3) + 4.*EK(2) - 3.*EK) /DEL2
  EMTp = (-EMT(3) + 4.*EMT(2) - 3.*EMT) /DEL2
  IBCX = 0
  IF(EM1 .NE. 1.E+10) GO TO 20
  IBCX = EM1(2,1)
  IBM = 4439
C
  20 S9 = ENF /RHO
  S3 = GAM * D(I)
  S5 = D(I) /2. * S9
  OPEN TOP OR BOTTOM BOUND
00013040
00013050
00013060
00013070
00013080
00013090
00013100
00013120
00013130
00013140
00013150
00013160
00013170
00013180
00013190
00013200
00013210
00013220
00013230
00013240
00013250
00013260
00013270
00013280
00013290
00013300
00013310
00013320
00013330
00013340
00013350
00013360
00013370
00013380
00013390
00013400
00013410

```

S8 = S4 * S9 / 8. * S6 * S7	00013420
S15 = S4 * S9 / 2.	00013430
S9 = S9 ** 2	00013440
S10 = S4 * (S2 * GAM**2 * WFE(I) + S9/2. * S6)	00013450
S11 = S4 * S5 / D(I)	00013460
IF(IBCX .EQ. 0) GO TO 83	00013470
DO 22 K = 1, 32	00013480
IX = IBM + K	00013490
22 DA(IX) = 0.	00013500
GO TO (31, 32, 33, 34, 35), IBCX	00013510
C	00013520
31 DA(IBM+1) = 1.	00013530
DA(IBM+6) = 1.	00013540
DA(IBM+11) = 1.	00013550
DA(IBM+32) = 1.	00013560
GO TO 83	00013570
C	00013580
32 DA(IBM+1) = 1.	00013590
DA(IBM+22) = 1.	00013600
DA(IBM+27) = 1.	00013610
DA(IBM+32) = 1.	00013620
GO TO 83	00013630
C	00013640
33 DA(IBM+16) = 1.	00013650
DA(IBM+17) = 1.	00013660
DA(IBM+22) = 1.	00013670
DA(IBM+27) = 1.	00013680
GO TO 83	00013690
C	00013700
34 DA(IBM+17) = 1.	00013710
DA(IBM+22) = 1.	00013720
DA(IBM+27) = 1.	00013730
DA(IBM+32) = 1.	00013740
GO TO 83	00013750
C	00013760
35 DA(IBM+11) = 1.	00013770
DA(IBM+16) = 1.	00013780

C	83	DO	84	K = 1,4		00013790
		EM6(K)	=	0.		00013800
		DO	84	L = 1,4		00013810
		EM2(K,L)	=	0.		00013820
	84	EM4(K,L)	=	0.		00013830
						00013840
						00013850
						00013860
						00013870
C	85	EM2(1,1)	=	D(I) / DEL		00013880
		EM4(1,1)	=	POI * S3		00013890
		EM4(1,2)	=	POI * ENF / RHO * D(I)		00013900
		EM4(1,3)	=	D(I) * (WFE(I) + POI*WTH)		00013910
		EM4(2,1)	=	-S5 * S1 - S8		00013920
		EM2(2,2)	=	D(I)*S1/2. + S4/8. * S7**2		00013930
		EM4(2,2)	=	- GAM * EM2(2,2)		00013940
		EM2(2,2)	=	EM2(2,2) / DEL		00013950
		EM2(2,3)	=	S15 * S7		00013960
		EM4(2,3)	=	- GAM * EM2(2,3)		00013970
		EM2(2,3)	=	EM2(2,3) / DEL		00013980
		EM4(3,1)	=	- S10		00013990
		EM2(3,2)	=	S11 * S7 / DEL		00014000
		EM4(3,2)	=	-S11 * GAM *(S7 + 2.*S2*WTH)		00014010
		EM2(3,3)	=	S4 * (2.*S9 + S2 * GAM **2) / DEL		00014020
		EM4(3,3)	=	-S4 *(3. + POI) * GAM * S9		00014030
		EM2(3,4)	=	ELAM2 / DEL		00014050
		EM4(3,4)	=	ELAM2 * S1 * GAM		00014060
		EM2(4,3)	=	- 1. / DEL		00014070
		EM4(4,1)	=	WFE(I)		00014080
		EM6(1)	=	- ENT(I)		00014090
		EM6(3)	=	ELAM2 * GAM * S1 * EMT(I)		00014100
		DO	90	K = 1,4		00014110
		DO	90	L = 1,4		00014120
	90	EM2(K,L)	=	- EM2(K,L) / 2.		00014130
		GO	TO	121		00014140
C	95	IF(RESTRT .NE. 0.) GO TO 94				00014150
		TOP BOUNDARY, CLOSED				00014160


```

IF(TIME .NE. TDEL) GO TO 97
94 DO 96 K = 1,4
DO 96 L = 1,4
EM1(K,L) = EM2(K,L)
96 EM3(K,L) = EM4(K,L)
RESTR = 0.
97 DO 98 K = 1,4
G2(K) = 0.
DO 98 L = 1,4
A2(K,L) = 2. * EM1(K,L)
C2(K,L) = -.25 * A2(K,L)
98 EM1(K,L) = 1.5 * EM1(K,L)
CALL MSU (4,4, EM3,EM1,B2)
GO TO 300
100 IF(I - N) 102,101,102
101 BP = (D(N-2) - 4.*D(N-1) + 3.*D(N)) /DEL2
WFEP = (WFE(N-2) - 4.*WFE(N-1) + 3.*WFE(N)) /DEL2
DP = (EK(N-2) - 4.*EK(N-1) + 3.*EK(N)) /DEL2
TTP = (ENT(N-2) - 4.*ENT(N-1) + 3.*ENT(N)) /DEL2
EMTP = (EMT(N-2) - 4.*EMT(N-1) + 3.*EMT(N)) /DEL2
IBCX = 0
IF(EMIN .NE. 1.E+10) GO TO 20
IBCX = EMIN(2,1)
IBM = 4475
GO TO 20

C
102 BP = (D(I+1) - D(I-1)) /DEL2
WFEP = (WFE(I+1) - WFE(I-1)) /DEL2
DP = (EK(I+1) - EK(I-1)) /DEL2
TTP = (ENT(I+1) - ENT(I-1)) /DEL2
EMTP = (EMT(I+1) - EMT(I-1)) /DEL2

ALL EXCEPT CLOSED APEX

C
120 S3 = GAM * D(I)
S5 = D(I) /2. * ENF /RHO
S8 = S4 * ENF /8. /RHO * S6 * S7
S9 = (ENF /RHO) **2
S10 = S4 * (S2 * GAM**2 * WFE(I) + S9/2. * S6)

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00014170
00014180
00014190
00014200
00014210
00014220
00014230
00014240
00014250
00014260
00014270
00014280
00014290
00014300
00014310
00014320
00014330
00014340
00014350
00014360
00014370
00014380
00014390
00014400
00014410
00014420
00014430
00014440
00014450
00014460
00014470
00014480
00014490
00014500
00014510
00014520
00014530

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C      S11 = S4 * S5 / D(I)
      121 DO 125 K = 1,4
      DO 125 L = 1,4
      125 E(K,L) = 0.
      E(1,1) = D(I) / DEL
      F(1,1) = S3 + BP
      S12 = WTH * WFE(I)
      GAM2 = GAM **2
      GA(1,1) = POI * BP * GAM - D(I) * (POI * S12 + GAM2 + S1 * S9 / 2.)
      1 - S4 * (S2 * GAM2 * WFE(I) **2 + S6 **2 * S9 / 8.)
      F(1,2) = S2 * S5 + S8
      GA(1,2) = POI * ENF / RHO * BP - (3. - POI) * S5 * GAM - S11 * 2.
      1 * GAM * (S6 * S7 / 8. + S2 * S12)
      F(1,3) = D(I) * (WFE(I) + POI * WTH) + S10
      GA(1,3) = D(I) * (WFE(I) + GAM * (WFE(I) - WTH)) + BP * (WFE(I) + POI *
      1 WTH) - S4 * S9 * GAM * (S6 / 2. + S2 * WFE(I))
      F(1,4) = ELAM2 * WFE(I)
      GA(1,4) = F(1,4) * S1 * GAM
      F(2,1) = - F(1,2)
      GA(2,1) = - S5 * GAM * (3. - POI) - S1 * ENF / 2. * BP / RHO + S11 * 2.
      1 * (- S2 * GAM * S12 + GAM / 8. * (6. * S12 - 7. * WFE(I) **2 - 3. * WTH
      2 **2) - WFE(I) / 4. * (5. * WTH - 3. * WFE(I)) - S11 * DP / EK(I) / 4. * S6 * S7
      E(2,2) = (D(I) / 2. * S1 + S4 / 8. * S7 **2) / DEL
      F(2,2) = S1 / 2. * (GAM * D(I) + BP) - S4 / 8. * S7 * (2. * WFEP - GAM
      1 * (5. * WFE(I) - 3. * WTH)) + ELAM2 / 8. * DP * S1 * S7 **2
      GA(2,2) = - GAM * F(2,2) + D(I) * (S1 / 2. * S12 - S9) - S4 * (S2 * S9
      1 * WTH **2 - S12 / 8. * S7 **2)
      E(2,3) = S11 * S7 / DEL
      F(2,3) = S11 * (2. * S2 * GAM * WTH - WFEP + 3. * GAM * (WFE(I) -
      1 WTH)) + S11 / EK(I) * DP * S7
      GA(2,3) = - S5 * 2. * (WTH + POI * WFE(I)) + S4 * S5 / D(I) * (GAM *
      1 WFEP - 2. * GAM2 * WFE(I) - 2. * S2 * S9 * WTH + S7 * (GAM2 + S12)) - S11 /
      2 EK(I) * DP * GAM * S7
      GA(2,4) = - POI * ELAM2 * WTH * ENF / RHO
      F(2,4) = 0.
      F(3,1) = - F(1,3)
      00014540
      00014550
      00014560
      00014570
      00014580
      00014590
      00014600
      00014610
      00014620
      00014630
      00014640
      00014650
      00014660
      00014670
      00014680
      00014690
      00014700
      00014710
      00014720
      00014730
      00014740
      00014750
      00014760
      00014770
      00014780
      00014790
      00014800
      00014810
      00014820
      00014830
      00014840
      00014850
      00014860
      00014870
      00014880
      00014890
      00014900

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S13 = WTH + POI*WFE(I)
GA(3,1) = -D(I)*GAM * S13 + ELAM2*EK(I)*S1 *( GAM * S2 *(GAM2
1 *WFE(I) - GAM * WFEP - WFE(I) *(S9 - 2.*S12)) + S9/2. *(GAM
2 *(WFE(I) - WTH) - 3.*WFEP) - ELAM2*DP*S1 *(S2*GAM2*WFE(I) + S9
3 /2. * S6)
E(3,2) = E(2,3)
F(3,2) = S11 *( GAM *( WFE(I)*3. -WTH*(5. + 2.*POI)) - WFEP)
1 + S11*DP/EK(I) * S7
GA(3,2) = -D(I)*ENF /RHO * S13 + S11 *(2.*S2 *(S12*WTH - GAM2 *
1 (WFE(I) - 2.*WTH) - S9*WTH) + GAM * WFEP + 3.*GAM2*(WTH - WFE(I))*00015000
2 ) + S12*S7) - S11*DP/EK(I) *( GAM *(2.*S2*WTH + S7) )
E(3,3) = S4 *(2.*S9 + S2*GAM2) /DEL
F(3,3) = -S4*(S2*GAM *(2.*S12 + GAM2) + 2.*GAM * S9) + ELAM2
1 *DP*S1 *(S2*GAM2 + 2.*S9)
GA(3,3) = -O(I) *(WFE(I)**2 + 2.*POI*S12*WTH**2)+S4*S9*(S2*(S12-00015050
1 S9 + 2.*GAM2) + 2.*(GAM2 + S12)) - S1*S9*DP*ELAM2 *(3.*POI)*GAM
E(3,4) = ELAM2 /DEL
F(3,4) = ELAM2 * GAM *(2. - POI)
GA(3,4) = - ELAM2 * (S1*S12 + POI*S9)
F(4,1) = EK(I) * WFE(I)
GA(4,1) = EK(I) *(WFEP + POI*GAM*WFE(I))
GA(4,2) = EK(I) * POI*ENF*WTH /RHO
E(4,3) = -EK(I) /DEL
F(4,2) = 0.
F(4,3) = -EK(I) * POI * GAM
F(4,4) = 0.
GA(4,3) = EK(I) * POI * S9
140 GA(1,1) = GA(1,1) - S77 * SKFE
GA(3,3) = GA(3,3) - S77 * SKZ
IF(I .NE. N2) GO TO 142
S3 = A0 /EO * A0 /HO
GA(1,1) = GA(1,1) - UK * S3
GA(2,2) = GA(2,2) - VK * S3
GA(3,3) = GA(3,3) - WK * S3
S3 = S3 /AO * EMK * WFE(I)
F(1,3) = F(1,3) - S3
GA(1,1) = GA(1,1) + S3 * WFE(I)
00014910
00014920
00014930
00014940
00014950
00014960
00014970
00014980
00014990
00015000
00015010
00015020
00015030
00015040
00015050
00015060
00015070
00015080
00015090
00015100
00015110
00015120
00015130
00015140
00015150
00015160
00015170
00015180
00015190
00015200
00015210
00015220
00015230
00015240
00015250
00015260
00015270

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142 GA(4,4) = - 1.
G(1) = (-PFE(I) + TTP - ELAM2 *S1*GAM*WFE(I)*EMT(I)) * DEL2
G(2) = (-PTH(I) - ENF/RHO*(ENT(I)+ ELAM2*S1*WTH*EMT(I)))*DEL2
G(3) = (-PN(I) - (WFE(I) + WTH)*ENT(I) - ELAM2*S1 *(GAM*EMTP
1 - EMT(I) * (S12 - S9) )) * DEL2
G(4) = EMT(I) * DEL2
DO 150 K = 1,4
DO 150 L = 1,4
150 F(K,L) = 2. * E(K,L)
CALL MAD (4,4, E,F,A)
CALL MSU (4,4, E,F,C)
DO 160 K = 1,4
DO 160 L = 1,4
E(K,L) = - 2. * E(K,L)
160 GA(K,L) = DEL2 * GA(K,L)
CALL MAD (4,4, E,GA,B)
DO 162 K = 1,4
G(K) = G(K) * TDEL
DO 162 L = 1,4
A(K,L) = A(K,L) * TDEL
B(K,L) = B(K,L) * TDEL
162 C(K,L) = C(K,L) * TDEL
IF(JT - 2) 163,164,165
163 S79 = -6. * OMG2(I)
S80 = 6.
GO TO 166
164 LM11 = S80 + 5.3333333 * BTA11
LM22 = S80
LM33 = S80 + 5.3333333 * BTA33
165 S79 = -2. * OMG2(I)
S80 = 11. /3.
166 B(1,1) = B(1,1) + S79 + S80 * BTA11
B(2,2) = B(2,2) + S79
B(3,3) = B(3,3) + S79 + S80 * BTA33
G(1) = G(1) + LM11*ZP(1,I) + MM11*Z2P(1,I) + NM11*Z3P(1,I)
G(2) = G(2) + LM22*ZP(2,I) + MM22*Z2P(2,I) + NM22*Z3P(2,I)
G(3) = G(3) + LM33*ZP(3,I) + MM33*Z2P(3,I) + NM33*Z3P(3,I)

```

00015280
00015290
00015300
00015310
00015320
00015330
00015340
00015350
00015360
00015370
00015380
00015390
00015400
00015410
00015420
00015430
00015440
00015450
00015460
00015470
00015480
00015490
00015500
00015510
00015520
00015530
00015540
00015550
00015560
00015570
00015580
00015590
00015600
00015610
00015620
00015630
00015640

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IF(I - 2) 210,170,169
169 IF(I - N) 185,200,185
C
170 CALL INV (4, C, PI, IERR)
CALL MMY (4,4,4, B2,C,EM4)
CALL MMY (4,4,4, EM4,B,B2)
CALL MSU (4,4, B2,A2,B2)
CALL INV (4, B2, PI, IERR)
IF(EN1 - 2.) 176,172,172
172 CALL MMY (4,4,4, EM4,A,A2)
CALL MSU (4,4, A2,C2,A2)
CALL MMY (4,4,4, B2,A2,P(1,1,2))
GO TO 178
176 CALL MMY (4,4,4, B2,EM4,A2)
CALL MMY (4,4,4, A2,A,P(1,1,2))
178 CALL MMY (4,4,1, EM4,G,EM6)
CALL MSU (4,1, EM6,G2,G2)
CALL MMY (4,4,1, B2,G2,X(1,2))
C
DO 180 K = 1,4
G2(K) = G(K)
DO 180 L = 1,4
A2(K,L) = A(K,L)
B2(K,L) = B(K,L)
180 C2(K,L) = C(K,L)
GO TO 300
185 CALL MMY (4,4,4, C,P(1,1,I-1),EM4)
CALL MSU (4,4, B,EM4,EM4)
CALL INV (4, EM4, PI, IERR)
CALL MMY (4,4,1, C,X(1,I-1),EM6)
CALL MSU (4,1, G,EM6,EM6)
IF(I - N) 190,220,190
190 CALL MMY (4,4,4, EM4,A,P(1,1,I))
CALL MMY (4,4,1, EM4,EM6,X(1,I))
GO TO 300
C
200 CALL INV (4, A, PI, IERR)

```

I = 2

I = N

217 E(K,L) = 0.		00016400
GO TO 300		00016410
220 CALL MMY (4,4,1, EM4,EM6,Z(1,N))		00016420
300 CONTINUE		00016430
C	DEFLECTIONS	00016440
DO 305 I = 1,N		00016450
IZ = N - I		00016460
IF(IZ - 1) 304,310,304		00016470
304 CALL MMY (4,4,1, P(1,1,IZ),Z(1,IZ+1),EM6)		00016480
305 CALL MSU (4,1, X(1,IZ),EM6,Z(1,IZ))		00016490
C	I = 1	00016500
310 CALL MMY (4,4,1, B2,Z(1,2),EM6)		00016510
CALL MSU (4,1, G2,EM6,G2)		00016520
CALL MMY (4,4,1, A2,Z(1,3),EM6)		00016530
CALL MSU (4,1, G2,EM6,G2)		00016540
CALL MMY (4,4,1, C2,G2,Z(1,1))		00016550
C		00016560
1000 RETURN		00016570
END		00016580

	DECK NO. 8K-904	
\$IBFTC MSUB		00002110
C MATRIX SUBTRACT SUBROUTINE		00002120
C		00002130
C ARGUMENTS		00002140
C L NO. OF ROWS		00002150
C M NO. OF COLS		00002160
C A(I,J) MRA		00002170
C B(I,J) MSU		00002180
C C(I,J) MSR		00002190
C SUBROUTINE MSU(L,M,A,B,C)		00002200
DIMENSION A(4,4), B(4,4), C(4,4)		00002210
DO 30 I=1,L		00002220
DO 30 J=1,M		00002230
30 C(I,J)=A(I,J)-B(I,J)		00002240
RETURN		00002250
END		00002260

\$IBFTC INVR\$				00016590
C	MATRIX INVERSION SUBROUTINE	DECK NO. 8K-900		00016600
C				00016610
C	MODIFICATION OF F1,4B444 BY D.J.HALLMAN,DEPT. 56,LA			00016620
C				00016630
C	ARGUMENTS			00016640
C	IOM	INDICATOR OF ORDER (N) OF MATRIX A	COMPILED FOR 4 X 4	00016650
C	IERR	INDICATOR OF ERROR RETURN	=1,NORMAL. NOT=1,ERR	00016660
C				00016670
C	MATRICES			00016680
C	A(I,J)	INPUT MATRIX		00016690
C	LR(M)	MATRIX OF LOCATIONS OF MAX ROW	N,N	00016700
C	LC(M)	MATRIX OF LOCATIONS OF MAX COL	M,1	00016710
C			1,M	00016720
C	SUBSCRIPTS			00016730
C	I	ROW OF A		00016740
C	J	COL OF A		00016750
C	MI	LOCATION OF PIVOT BEFORE INTERCHANGE,ROW OF MAX		00016760
C	MJ	LOCATION OF PIVOT BEFORE INTERCHANGE,COL OF MAX		00016770
C	M	LOCATION OF PIVOT,ROW AND COL		00016780
C	N	ORDER OF MATRIX		00016790
C				00016800
C	VARIABLES			00016810
C	P	PIVOT ELEMENT,MAX ELEMENT BEFORE INTERCHANGE		00016820
C	PI	PI PRODUCT OF P(M) =VALUE OF DETERMINANT		00016830
C				00016840
C	TEMPORARY			00016850
C	TEMP	INTERCHANGE AND REORDERING OF ELEMENTS OF A		00016860
C				00016870
C		*	*	00016880
C			*	00016890
C				00016900
C				00016910
C	SETUP			00016920
C				00016930
C				00016940
C				00016950

SUBROUTINE INVT(IOM,A,PI,IERROR)
 DIMENSION A(4,4), LR(4), LC(4)
 SETUP
 M=1
 N=IOM
 PI=1.0


```

C      SEARCH REDUCED ARRAY FOR MAXIMUM ELEMENT
1000 P=0.0
      DO 1010 I=M,N
      DO 1010 J=M,N
      IF( ABS(P) - ABS( A(I,J) ) ) 1005,1010,1010
1005 P=A(I,J)
      MI=I
      MJ=J
1010 CONTINUE
      LR(M)=MI
      LC(M)=MJ
C      INTERCHANGE MAXIMUM ROW WITH PIVOT ROW
2000 IF(MI-M)2100,2200,2100
2100 DO 2110 J=1,N
      TEMP=A(MI,J)
      A(MI,J)=A(M,J)
      A(M,J)=TEMP
2110 A(M,J)=TEMP
C      INTERCHANGE MAXIMUM COL WITH PIVOT COL
2200 IF(MJ-M)2205,3000,2205
2205 DO 2210 I=1,N
      TEMP=A(I,MJ)
      A(I,MJ)=A(I,M)
      A(I,M)=TEMP
2210 A(I,M)=TEMP
C      DIVIDE PIVOT COL BY PIVOT ELEMENT
3000 DO 3010 I=1,N
      IF(I-M)3005,3010,3005
3005 A(I,M)=-A(I,M)/P
3010 CONTINUE
C      ELIMINATE
4000 DO 4210 I=1,N
      IF(I-M)4005,4210,4005
4005 DO 4110 J=1,N
      IF(J-M)4105,4110,4105
4105 A(I,J)=A(I,M)*A(M,J)+A(I,J)
4110 CONTINUE
4210 CONTINUE
C      DIVIDE PIVOT ROW BY PIVOT ELEMENT

```

```

00016960
00016970
00016980
00016990
00017000
00017010
00017020
00017030
00017040
00017050
00017060
00017070
00017080
00017090
00017100
00017120
00017130
00017140
00017150
00017160
00017170
00017180
00017190
00017200
00017210
00017220
00017230
00017240
00017250
00017260
00017270
00017280
00017290
00017300
00017310
00017320
00017330

```

5000 DO 5010 J=1,N	00017340
IF(J-M)5005,5010,5005	00017350
5005 A(M,J)=A(M,J)/P	00017360
5010 CONTINUE	00017370
C FORM DETERMINANT	00017380
PI=P*PI	00017390
A(M,M)=1.0/P	00017400
M=M+1	00017410
IF(M-N)1000,5020,5999	00017420
5020 P=A(M,M)	00017430
GO TO 3000	00017440
5999 M=N-1	00017450
6000 MI=LC(M)	00017460
MJ=LR(M)	00017470
C RE-ORDER ROWS OF INVERSE	00017480
IF(MI-M)6005,6200,6005	00017490
6005 DO 6010 J=1,N	00017500
TEMP=A(M,J)	00017510
A(M,J)=-A(MI,J)	00017520
6010 A(MI,J)=TEMP	00017530
C RE ORDER COLS OF INVERSE	00017540
6200 IF(MJ-M)6205,7000,6205	00017550
6205 DO 6210 I=1,N	00017560
TEMP=A(I,M)	00017570
A(I,M)=-A(I,MJ)	00017580
6210 A(I,MJ)=TEMP	00017590
7000 M=M-1	00017600
IF(M)9002,9001,6000	00017610
9001 ERROR=1	00017620
GO TO 9999	00017630
C M IS LESS THAN ZERO	00017640
9002 ERROR=2	00017650
9999 RETURN	00017660
END	00017670

IF(JT.EQ. NJT) GO TO 90	00018060
SL1 = 1.	00018070
IF(DRW.EQ. 0.) GO TO 50	00018080
SL1 = -1.	00018090
GO TO 90	00018100
C	00018110
50 JT = JT + 1	00018120
DO 60 I = 1,N	00018130
DO 60 J = 1,3	00018140
Z3P(J,I) = Z2P(J,I)	00018150
Z2P(J,I) = ZP(J,I)	00018160
60 ZP(J,I) = Z(J,I)	00018170
C	00018180
80 RETURN	00018190
C	00018200
90 S3 = 11.	00018210
S4 = 18.	00018220
S5 = 2.	00018230
S6 = 5.	00018240
S9=9.	00018250
S10=2.	00018260
S11=4.	00018270
S12=1.	00018280
IF(JT - 2) 100,110,120	00018290
100 S3=6.	00018300
S4=6.	00018310
S9=0.	00018320
S10=0.	00018330
S5=0.	00018340
S6=0.	00018350
S11=0.	00018360
S12=0.	00018370
GO TO 120	00018380
110 S3=6.	00018390
S4=6.	00018400
S9=0.	00018410
S10=0.	00018420

COMPUTE VELOCITIES, ACCELER.

```

S5=1.
S6=2.
S11=1.
S12=0.

120 S7 = 6. * TDEL
    TDEL2 = TDEL **2
    DO 150 L = 1,N
    DO 150 K = 1,3
    ZDOT(K,L) = (S3 * Z(K,L) - S4 * ZP(K,L) + S9 * Z2P(K,L) -
1      S10 * Z3P(K,L)) / S7
    150 Z2DOT(K,L) = (S5 * Z(K,L) - S6 * ZP(K,L) + S11 * Z2P(K,L) -
1      S12 * Z3P(K,L)) / TDEL2
    IF(JT.GT.1) GO TO 170
    DO 160 L=1,N
    ZDOT(1,L)= ZDOT(1,L) /TDEL
    Z2DOT(2,L)=0.
    160 Z2DOT(3,L)= ZDOT(3,L) /TDEL
170 CONTINUE
C

IF(SL1 .LT. 0.) GO TO 300
IF(JT .EQ. NJT) GO TO 200
PRNT = PRNT + PRI
GO TO 50

C      SET UP NEW INTERVAL
200 IF(TAU1 + TAU2 - TIMX .LE. 1.E-8) GO TO 210
C      SECOND

    TDEL = TAU2 /ENT2
    PRNT = PI2
    NJT = ENT2
    PRI = PI2
    TIMX = TAU1
    GO TO 220

C      THIRD
210 IF(TAU1 + TAU2 + TAU3 - TIMX .LE. 1.E-8) GO TO 50
    TDEL = TAU3 /ENT3
    PRNT = PI3
    NJT = ENT3

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00018430
00018440
00018450
00018460
00018470
00018480
00018490
00018500
00018510
00018520
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00018540
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00018560
00018570
00018580
00018590
00018600
00018610
00018620
00018630
00018640
00018650
00018660
00018670
00018680
00018690
00018700
00018710
00018720
00018730
00018740
00018750
00018760
00018770
00018780
00018790

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```

      PRI = PI3
      TIMX = TAU2 + TAU1
C
      220 JT = 1
          TDEL2 = TDEL **2
          DO 250 K = 1,3
          DO 250 I = 1,N
          IF(K - 2) 231,232,233
      231 S8 = PFE(I) /MO(I)
          GO TO 240
      232 S8 = 0.
          GO TO 240
      233 S8 = PN(I) /MO(I)
      240 ZP(K,I) = Z(K,I)
          Z2P(K,L) = S8 * TDEL2 + 2. * Z(K,L)
      250 Z3P(K,L) = 6. * (S8 * TDEL2 + ZDOT(K,L) * TDEL) + 9. * Z(K,L)
          GO TO 80
C
      300 WRITE (6,310) ((ZDOT(K,L), K=1,3), (Z2DOT(K,L), K=1,3), L=1,N)
      310 FORMAT(///10X,28HVELOCITIES AND ACCELERATIONS // 15X,6HVEL(U),
          1 10X,6HVEL(V), 10X,6HVEL(W), 10X,6HACC(U), 10X,6HACC(V), 10X,
          2 6HACC(W) // (6X, 1P6E16.3) )
C
          GO TO 50
      END
00018800
00018810
00018820
00018830
00018840
00018850
00018860
00018870
00018880
00018890
00018900
00018910
00018920
00018930
00018940
00018950
00018960
00018970
00018980
00018990
00019000
00019010
00019020
00019030
00019040

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4 S77, S78, BTA11, BTA33, MO(200), OMG2(200), ZP(3,200), 00019620
5 Z2P(3,200), Z3P(3,200), TIMX, TDEL, PRNT, ENF, PRI, JT, NJT, V1 00019630
COMMON 00019640
1 USUM, VSUM, WSUM, EMFE, EMTH, EMFI, ENFE, ENTH, ENFI, SIGFE, 00019650
2 SIGTH, SIGFT, QFE, QTH 00019660
C 00019670
C 00019680
C 00019690
C 00019700
C 00019710
C 00019720
C 00019730
C 00019740
C 00019750
C 00019760
C 00019770
C 00019780
C 00019790
C 00019800
C 00019810
C 00019820
C 00019830
C 00019840
C 00019850
C 00019860
C 00019870
C 00019880
C 00019890
C 00019900
C 00019910
C 00019920
C 00019930
C 00019940
C 00019950
C 00019960
C 00019970
C 00019980

      COMPUTE INTERNAL LOADS

490 S3 = 1. - POI **2
S4 = S1 / 2.
S12 = SIGO / EO / S3
S20 = (HO / AO) **2
IF(EN1 - 2.) 496,497,497
496 L1 = 1
GO TO 498
497 L1 = 2
WP = (-Z(3,3) + 4.*Z(3,2) - 3.*Z(3,1)) / DEL2
FETH(1) = ENF * WP + WTHD * Z(2,1)
498 DO 500 I = L1,N
500 FETH(I) = ENF / RHOX(I) * Z(3,1) + WTHD(I) * Z(2,1)
502 DO 1000 I = 1,N
IF(I - 1) 520,504,520
504 IF(EN1 - 2.) 510,506,506
506 ENFEX = D(1) * ((S2*(Z(1,2) - Z(1,1)) + ENF*POI*(Z(2,2) - Z(2,1))) / DEL
1) / DEL + WFE * S2 * Z(3,1)) - ENT
S6 = 2. - ENF **2
ENTHX = 2. * ENFEX / S6
ENFTX = ENF * ENFEX / S6
EMFTX = ENF * Z(4,1) / S6
EMTHX = 2.0 * Z(4,1) / S6
GO TO 552

C
510 ROP = (-RHOX(3) + 4. * RHOX(2) - 3. * RHOX(1)) / DEL2
WP = (-Z(3,3) + 4. * Z(3,2) - 3. * Z(3,1)) / DEL2
FETHP = (-FETH(3) + 4.*FETH(2) - 3. * FETH(1)) / DEL2
VP = (-Z(2,3) + 4. * Z(2,2) - 3. * Z(2,1)) / DEL2
UP = (-Z(1,3) + 4. * Z(1,2) - 3. * Z(1,1)) / DEL2
EM6(4) = (-Z(4,3) + 4. * Z(4,2) - 3. * Z(4,1)) / DEL2

```



```

515 EM6(2) = VP
EM6(3) = WP
EM6(1) = UP
GO TO 550
520 IF(I - N) 540,530,540
C
530 WP = (Z(3,N-2) - 4.*Z(3,N-1) + 3.*Z(3,N)) / DEL2
FETHP = (FETH(N-2) - 4.*FETH(N-1) + 3.*FETH(N)) / DEL2
VP = (Z(2,N-2) - 4.*Z(2,N-1) + 3.*Z(2,N)) / DEL2
UP = (Z(1,N-2) - 4.*Z(1,N-1) + 3.*Z(1,N)) / DEL2
EM6(4) = (Z(4,N-2) - 4.*Z(4,N-1) + 3.*Z(4,N)) / DEL2
ROP = (RHOX(N-2) - 4.*RHOX(N-1) + 3.*RHOX(N)) / DEL2
GO TO 515
C
540 WP = (Z(3,I+1) - Z(3,I-1)) / DEL2
FETHP = (FETH(I+1) - FETH(I-1)) / DEL2
ROP = (RHOX(I+1) - RHOX(I-1)) / DEL2
VP = (Z(2,I+1) - Z(2,I-1)) / DEL2
UP = (Z(1,I+1) - Z(1,I-1)) / DEL2
EM6(4) = (Z(4,I+1) - Z(4,I-1)) / DEL2
GO TO 515
550 FEFE = - WP + WFE(I) * Z(1,I)
X(3,I) = FEFE
S11 = ENF / RHOX(I)
S5 = S11 * Z(2,I) + GAMA(I) * Z(1,I) + WTHD(I) * Z(3,I)
S6 = UP + WFE(I) * Z(3,I)
EKTH = S11 * FETH(I) + GAMA(I) * FEFE
ENFEX = D(I) * (S6 + POI * S5) - ENT(I)
EMTHX = POI * Z(4,I) + EK(I) * S3 * EKTH - S1 * EMT(I)
ENTHX = D(I) * (S5 + POI * S6) - ENT(I)
ENFTX = D(I) * S4 * (VP - GAMA(I) * Z(2,I) - S11 * Z(1,I))
EMFTX = EK(I) * S4 * (-S11 * FEFE + FETHP - GAMA(I) * FETH(I) + .5 *
1 (WTHD(I) - WFE(I)) * (S11 * Z(1,I) + VP + GAMA(I) * Z(2,I)) )
552 S15 = DNA(I) / A0
S7 = S15 * S3
S9 = E1(I) * ALF(I) * T(I) / S1
S8 = S12 * E1(I)

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00019990
00020000
00020010
00020020
00020030
00020040
00020050
00020060
00020070
00020080
00020090
00020100
00020110
00020120
00020130
00020140
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00020170
00020180
00020190
00020200
00020210
00020220
00020230
00020240
00020250
00020260
00020270
00020280
00020290
00020300
00020310
00020320
00020330
00020340
00020350

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S10 = S8 * S15 * EMT(I) / EK(I)	00020360
IF(RHOX(I)) 551,555,551	00020370
551 IF(I - 1) 554,553,554	00020380
553 S13 = 2.	00020390
GO TO 559	00020400
554 S13 = 1.	00020410
GC TO 559	00020420
555 S6 = S15 / EK(I) * (Z(4,1) + EMT(I))	00020430
S11 = (Z(2,2) - Z(2,1)) / DEL	00020440
S13 = (Z(1,2) - Z(1,1)) / DEL	00020450
IF(ENF - 1.) 556,557,558	00020460
556 G(1) = S8 * (S2 * (S13 + WFE * Z(3,1)) + S6) - S9	00020470
G(2) = G(1)	00020480
G(3) = 0.	00020490
GO TO 578	00020500
557 G(1) = S8 * (POI * S11 + S6 / POI) - S9	00020510
G(2) = S8 * (S11 + S6 / POI) - S9	00020520
G(3) = 0.	00020530
GO TO 578	00020540
558 G(1) = S8 * (S2 * S13 + POI * ENF * S11 + S6) - S9	00020550
G(2) = S8 * (S2 * S13 + ENF * S11 + S6 / POI) - S9	00020560
G(3) = S8 * ENF * (S15 / (2. - ENF * 2) * Z(4,1) / EK(1) - S13 * S1 / 2.)	00020570
GO TO 578	00020580
559 S6 = S4 * (S15 / 2. * (3. * WTHD(I) - WFE(I)) + 1.)	00020590
QFEX = S20 * (GAMA(I) * (Z(4,1) - EMTX) + EM6(4) + ENF / RHOX(I) *	00020600
1 EMTX * S13)	00020610
565 DO 560 K = 1,3	00020620
DO 560 L = 1,4	00020630
560 EM4(K,L) = 0.	00020640
EM4(1,1) = S8	00020650
EM4(2,1) = POI * S8	00020660
EM4(2,3) = - S7 * GAMA(I) * S8	00020670
EM4(3,2) = S6 * S8	00020680
EM4(3,3) = S15 * S1 * S11 * S8	00020690
G2(1) = S10 - S9	00020700
G2(2) = POI * S10 - S9	00020710
G2(3) = 0.	00020720

```

      B2(1,1) = POI * GAMA(I) * S8
      B2(1,2) = POI * S11 * S8
      B2(1,3) = (WFE(I) + POI * WTHD(I)) * S8
      B2(1,4) = S15 / EK(I) * S8
      B2(2,1) = GAMA(I) * (1. + S7*WFE(I)) * S8
      B2(2,2) = S8 * S11 * (1. + S7*WTHD(I))
      B2(2,3) = S8 * (WTHD(I) + POI*WFE(I) + S7 * S11 **2)
      B2(2,4) = B2(1,4) * POI
      B2(3,1) = S8 * S4 * S11 * (S15/2. * (WTHD(I) - 3.*WFE(I)) - 1.)
      B2(3,2) = - EM4(3,2) * GAMA(I)
      B2(3,3) = - S8 * S1 * S11 * S15 * GAMA(I)
      B2(3,4) = 0.
      CALL MMY (3,4,1,EM4,EM6,G)
      CALL MMY (3,4,1,B2,Z(1,1),EC)
      CALL MAD (3,1,G,EC,G)
      CALL MAD (3,1,G,G2,G)

C 578 USUM(I) = Z(1,1)
      VSUM(I) = Z(2,1)
      WSUM(I) = Z(3,1)
      EMFE(I) = Z(4,1)
      EMTH(I) = EMTHX
      EMFT(I) = EMFTX
      ENFE(I) = ENFEX
      ENTH(I) = ENTHX
      ENFT(I) = ENFTX
      SIGFE(I) = G(1)
      SIGTH(I) = G(2)
      SIGFT(I) = G(3)
      QFE(I) = QFEX
      X(1,1) = 2. * ROP * EMFTX - ENF * EMTHX
      X(2,1) = EMFTX
1000 CONTINUE
      DO 599 I = 1,N
      IF(I.NE. 1) GO TO 593
      EMFTP = (EMFT(2) - EMFT(1)) / DEL
      IF( RHOX(I) ) 596,592,596

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SAVE FOURIER COEFFICIENTS

	I = 1, CLOSED APEX	
C 592 EMFEP = (EMFE(2) - EMFE(1)) / DEL	00021100	
EMTHP = (EMTH(2) - EMTH(1)) / DEL	00021110	
QFE(1) = ELAM2 * (EMFEP + ENF * EMFTP)	00021120	
QTH(1) = ELAM2 * (EMFTP - ENF * EMTHP)	00021130	
GO TO 599	00021140	
593 IF(I - N) 595,594,595	00021150	
594 EMFTP = (EMFT(N) - EMFT(N-1)) / DEL	00021160	
GO TO 596	00021170	
595 EMFTP = (EMFT(I+1) - EMFT(I-1)) / DEL2	00021180	
596 QTH(I) = ELAM2 / RHOX(I) * (X(I,1) + RHOX(I) * EMFTP)	00021190	
599 CONTINUE	00021200	
700 WRITE (8) (USUM(I), I = 1,2800)	00021210	
RETURN	00021230	
END	00021240	
	00021250	


```

3 SL1, SL2, N, NTH, NTPR, NTPW, I, K, L,
4 S77, S78, BTAIL, BTA33, MO(200), OMG2(200), ZP(3,200),
5 Z2P(3,200), Z3P(3,200), TIMX, TDEL, PRNT, ENF, PRI, JT, NJT, VI
COMMON
1 USUM, VSUM, WSUM, EMFE, EMTH, EMFT, ENFE, ENTH, ENFT, SIGFE,
2 SIGTH, SIGFT, QFE, QTH
C
705 S5 = ENF * THETA
COSNT = COS( S5 )
SINNT = SIN( S5 )
710 DO 720 I = 1,N
USUM(I) = USUM(I) * COSNT
VSUM(I) = VSUM(I) * SINNT
WSUM(I) = WSUM(I) * COSNT
EMFE(I) = EMFE(I) * COSNT
EMTH(I) = EMTH(I) * COSNT
EMFT(I) = EMFT(I) * SINNT
ENFE(I) = ENFE(I) * COSNT
ENTH(I) = ENTH(I) * COSNT
ENFT(I) = ENFT(I) * SINNT
SIGFE(I) = SIGFE(I) * COSNT
SIGTH(I) = SIGTH(I) * COSNT
SIGFT(I) = SIGFT(I) * SINNT
QFE(I) = QFE(I) * COSNT
QTH(I) = QTH(I) * SINNT
IF( SUM ) 755,755,758
C
730 WRITE (6, 733) TIMX, I, USUM(I), VSUM(I), WSUM(I),
1 EMFE(I), EMTH(I), EMFT(I), QFE(I), QTH(I), I = 1,N)
733 FORMAT(1H1,28X, 39HDEFLECTIONS AND INTERNAL LOADS, TIME =,1PE12.400021930
1 /// 3X,1H1, 5X,4HU(1), 9X,4HV(1), 9X,4HW(1), 8X,6HM(PHI), 6X,
2 8HM(THETA), 3X,12HM(PHI,THETA), 4X,6HQ(PHI), 6X,8HQ(THETA) //
3 (14, 8E13.4) )
WRITE
1 SIGTH(I), SIGFT(I),
735 FORMAT(1H1,2X,1H1, 4X,6HN(PHI), 6X,8HN(THETA), 3X,12HN(PHI,THETA), 00021990
1 3X,8HSIG(PHI), 4X,10HSIG(THETA), 2X,13HSG(PHI,THETA) //
00022000
00021640
00021650
00021660
00021670
00021680
00021690
00021700
00021710
00021720
00021730
00021740
00021750
00021760
00021770
00021780
00021790
00021800
00021810
00021820
00021830
00021840
00021850
00021860
00021870
00021880
00021890
00021900
00021910
00021920
00021930
00021940
00021950
00021960
00021970
00021980
00021990
00022000

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2 (I4, IP6E13.4) )
WRITE (6,738) ((ZDOT(K,L), K=1,3), (ZDOT(K,L), K=1,3), L=1,N)
738 FORMAT(///10X,28HVELOCITIES AND ACCELERATIONS // 15X,6HVEL(U),
1 10X,6HVEL(V), 10X,6HVEL(W), 10X,6HACC(U), 10X,6HACC(V), 10X,
2 6HACC(W) // (6X, IP6E16.3) )
C
740 IF( SUM ) 880,860,750
750 NTH = NTH - 1
IF( NTH ) 753,888,753
C
753 READ (NTPW) TIMX, THETA, (USUM(I), I = 1,2800)
755 S13 = AO * SIGO /EO
S14 = SIGO * HO **3 /AO
S16 = SIGO * HO
DO 756 I = 1,N
USUM(I) = S13 * USUM(I)
VSUM(I) = S13 * VSUM(I)
WSUM(I) = S13 * WSUM(I)
EMFE(I) = S14 * EMFE(I)
EMTH(I) = S14 * EMTH(I)
EMFT(I) = S14 * EMFT(I)
QFE(I) = S16 * QFE(I)
QTH(I) = S16 * QTH(I)
ENFE(I) = S16 * ENFE(I)
ENTH(I) = S16 * ENTH(I)
756 ENFT(I) = S16 * ENFT(I)
GO TO 730
C
758 IF( SL2 ) 810,820,810
810 NTH = NTH + 1
815 WRITE (NTPW) TIMX, THETA, (USUM(I), I = 1,2800)
GO TO 860
C
820 READ (NTPR) TIMX, THETA, (USUM(I), I = 1,2800)
DO 830 I = 1,2800
830 USUM(I) = USUM(I) + SUMN(I)
GO TO 815

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00022010
00022020
00022030
00022040
00022050
00022060
00022070
00022080
00022090
00022100
00022110
00022120
00022130
00022140
00022150
00022160
00022170
00022180
00022190
00022200
00022210
00022220
00022230
00022240
00022250
00022260
00022270
00022280
00022290
00022300
00022310
00022320
00022330
00022340
00022350
00022360
00022370

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860 CALL DECRD(DA)	00022380
IF(THETA) 880,880,865	00022390
865 REWIND 8	00022400
READ (8) (USUM(I), I = 1,2800)	00022410
GO TO 705	00022420
880 SL2 = 0.0	00022430
IF(TAU1 + TAU2 + TAU3 - TIMX .GT. 1.E-8) GO TO 890	00022440
REWIND NTPW	00022450
IF(ENFL - ENF .LE. 1.E-2) GO TO 900	00022460
887 NX = NTPR	00022470
NTPR = NTPW	00022480
NTPW = NX	00022490
888 SL1 = 1.	00022500
C 890 IF(DRW .NE. 0.) SL1 = -2.	00022510
RETURN	00022520
C	00022530
900 IF(SUM) 888,888,753	00022540
END	00022550
	00022560

\$18FTC LNK6				00022580
C 6J-148	** LNK6			00022590
C		PSEUDO CRT SUBROUTINE		00022600
	SUBROUTINE PIX			00022610
C				00022620
	LO = 0			00022630
	RETURN			00022640
	END			00022650